



Off Grid Energy Supply Solution

Sustainable Energy Solution for Off-Grid energy supply in the Kvarken Archipelago Vasa, Finland

Oriol Ala Puig

Tim Eebes

Christophe Hopchet

Rida Lahmaidi

Hui Liang

Simon Lillqvist

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Project report

Authors: Oriol Ala Puig, Tim Eebes, Christophe Hopchet, Rida Lahmaidi, Hui Liang, Simon Lillqvist

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Supervisors: Jan Teir and Bengt Englund

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Abstract

Today it is often diesel generators which provide the energy supply for remote islands in the archipelago. This project is about the development of a model for evaluation of energy needs but also to find a concept for replacing old generators by sustainable energy solution. The evaluation model was used to calculate the heat and electricity needs of two specific islands. The project included also the task to find a way to store excess energy. After comparing methods of storing energy, hydrogen fuel cells were found to have important advantages. They can store large amount of energy, are relatively cheap and are environmentally friendly. Solar and wind energy have been chosen as the main power sources. Sun and wind are widely known and available in the archipelago and obtaining energy out of these sources is known technology. The rare thing is the storage by hydrogen fuel cells. Storage by hydrogen fuel cells consists of four main stages: namely production, storage, utilization and reutilization.

This research shows that it is technically possible to use wind and solar power as main energy sources as well as storing energy in hydrogen fuel cells to create an autonomous off-grid power supply all year round.

Language: English

Keywords: Sustainable energy, fuel cell, archipelago

Projekt rapport

Författare: Oriol Ala Puig, Tim Eebes, Christophe Hopchet, Rida Lahmaidi, Hui liang, Simon Lillqvist

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Handledare: Jan Teir och Bengt Englund

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Abstrakt

Idag är det ofta dieselgeneratorer som sköter om energiförsörjningen för avlägsna öar i skärgården. Detta projekt handlar dels om att utveckla en modell för att utvärdera dylika energibehov och dels om att finna ett koncept för att ersätta gamla generatorer med hållbara energilösningar. I projektet används utvärderingsmodellen för att beräkna värme- och elektricitetsbehovet på två specifika öar. I projektet ingick också att finna ett sätt att lagra överskottsenergin. Efter att ha jämfört olika metoder för energilagring, visade det sig att vätgasbränsleceller har betydande fördelar. Vätgasbränslecellen kan lagra stora mängder energi samt är förhållandevis billig och miljövänlig. Sol- och vindenergi valdes som de primära energikällorna. Sol och vind är kända och tillgängliga källor i skärgården och att skapa energi ur dessa källor är välkänd teknik. Det som är mera ovanligt är energilagring i bränsleceller. Förvaring av energi tack vare vätebränsleceller innehåller fyra huvudsakliga steg, nämligen produktion, lagring, användning och återanvändning.

Denna forskning visar att det är tekniskt möjligt att använda vind- och solkraft som huvudsakliga energikällor samt att lagra energin i vätebränsleceller året om och på så sätt skapa en självständig och hållbar energiförsörjning.

Språk: Engelska

Nyckelord: Hållbar energi, bränslecell, skärgård

Summary

Introduction

This project is a research on the technological possibility to provide nature stations in the Kvarken archipelago with sustainable energy.

Archipelago

The Kvarken Archipelago, located southeast of Vasa in Finland, became Finland's first UNESCO Natural World Heritage Site in July 2007. (*kvarken.fi*) It is known as 'an internationally valuable natural area with many important habitats and endangered species. The area is characterised by its small scale and its biological and geomorphological diversity'. (*kvarkenguide.org (1)*) The archipelago consists of a group of islands. Some of those islands contain buildings. For example, Mickelsörarna, located northwest in the archipelago, has 'an old coast guard station, which was closed in 1993, now serves as a nature station' (*kvarkenguide.org(2)*). Valsörarna, located west of Mickelsörarna, is declared a bird sanctuary in 1948. Valsörarna's landmark, the red-painted 36-metre tall iron lighthouse, was designed in 1886 in Paris by the same firm that later built the Eiffel Tower. (*kvarkenguide.org (3)*). On Äbbskär, part of Valsörarna, there is also an old coast guard station.

Goals

Diesel generators supply the current power supply. This project consists of two main goals. Firstly, the development of a tool to evaluate the energy needs of the existing buildings. Secondly, the design of a sustainable, mostly autonomous solution that provides energy for the buildings on Mickelsörarna and Valsörarna. In this project sustainability denotes: minimal impact to the environment in the long-term. Not only the emissions of the system should be significantly lower than the current diesel system, the new solution should last about 20 years with low maintenance costs. The most autonomous factor refers to the fact that, the islands are inaccessible during the winter, due to the ice conditions.

The buildings have different energy needs. Valsörarna's coast guard station is bigger than the old coast guard station on Mickelsörarna. The building on Mickelsörarna has, a summer café. The electricity needs are for those reasons different. To develop a solution the electricity needs would have to be known. To calculate the needs the developed Energy Evaluation Model is used. The heating requirements of the buildings are similar. During the winter, the buildings need to be heated, to a stable five degrees Celsius. If the buildings experience high temperature fluctuations, the buildings will suffer from the climate and from falling into decay.

Possible energy sources

To produce sustainable energy in the archipelago there are different sources to exploit. Climate, weather, tide, waves and geothermal possibilities to generate energy from natural sources have been researched. The options were presented to the project owner and the project manager. During a project meeting all options were presented. During this meeting it was decided that Wind and Sun, with an energy backup by creating and storing hydrogen, would be the best possible sources to fulfill the energy needs throughout the year. In combination with a backup bio fuel generator, in case of complete system failure, this concept should provide an uninterrupted power supply throughout the year.

Primary System

As stated above there are three energy systems in this concept. The primary system contains a wind turbine and solar panels for the production of energy. The chosen wind turbine is a 12-meter tall, 10 kW turbine. In combination with a more specific chosen amount of solar panels the energy needs of the buildings are mostly covered. The combination of a wind turbine and solar panels is chosen on the weather data. In winter when the energy demand of the buildings is the highest, the wind is mostly stronger than in the summer. On Mickelsörarna where a café is open during the summer, solar panels are installed, as the average wind speeds are lower in the summer months, but the Solar Insolation is significantly bigger. When the demand of energy is bigger than the production, the stored hydrogen will supply the extra need. The hydrogen is created in times when the demand is lower then the production.

Secondary System

The excess energy that the main system produces is used to create hydrogen. Hydrogen is the source of backup energy when the main system output is not sufficient. Hydrogen is created out of purified water using an electrolyzer. The chemical reaction in the electrolyzer is:

 $2 H_2O(I) + Electricity (1.23 V) --> 2 H_2(g) + O_2(g)$

The created oxygen disperses into the air. The most adequate hydrogen storage system for the characteristics of this project (remote isolated location, automated, easy maintenance, safety, available space) is to use a pressurized steel tank containing gaseous hydrogen at no more than 30 bar.

- It is cheaper than other similar solutions, like composite tanks.
- It can operate at cold temperatures (liquid storage requires cryogenic temperatures).
- It doesn't require a heat input to extract the hydrogen (solid storage does).
- It is safe. In case of leakages, gaseous hydrogen dissipates easily in the air.

The backup system is designed so that it can supply non-stop energy for 7 days. To utilize the stored oxygen, a fuel cell is required. A Proton Exchange Membrane Fuel Cell is the most suitable for this project. Some advantages of a PEM FC are:

- Safer thanks to lack of hazardous chemicals
- Quick start-up
- Low temperature operation
- Few or no moving parts at all
- Maintenance becomes a less important issue
- They are scalable, from a small number of cells to a large stack depending on the need
- Efficiencies from 35 to 60 for electricity
- Efficiencies up to 85 or 90% for CHP (combined heat and power)

The chemical reaction in the Fuel Cell is:

 $2 H_2(g) + O_2(g) --> 2 H_2O(I)$

The electrolyzer needs to be fed water with a high grade of purity. This purified water needs to be transported and stored on the islands. The hydrogen is converted back to water vapor in the fuel cell. The water vapor can be retrieved to reuse it. It will run through a condenser and transported back to the purified water storage. It is in theory a closed cycle. In reality there will always be a certain level of losses. This makes it usable to size the purified water storage, not just big enough to fill the hydrogen tank, but a little bigger to take the losses into account.

Backup Generator

Due to the inaccessibility of the islands during the months when there is ice, the concept solution provides an emergency back-up generator. A control system is programmed that the generator will start automatically when both the primary and secondary system fail. It is a biofuel engine, designed for remote rural areas. It provides enough energy to keep the building heated to a stable 5 degrees Celsius.

Heating and ventilation

The heating system in the buildings on the islands is radiators on the wall with an inside water temperature of 45 degrees Celsius. The water is at the moment heated by generators. To heat up the water in the radiators a Heat pump will be installed. A vertical Ground Source Heat Pump is chosen for the following reason:

- There are no moving parts
- No view pollution
- No seasonal influence, therefore a stable temperature input
- High heat profit thanks to a high input temperature

Ventilation is another important factor for the prevention of structural damage on a building. Ventilation can happen naturally or mechanically. Naturally means that natural forces penetrate outside air into a building. Mechanical ventilation forces air in or out a building using electrically driven fans. Research on ventilation shows that the buildings in the archipelago benefit the most from a Heat Recovery Ventilation system. A heat exchanger transfers the heat of the outgoing air to the incoming air. This results in a substantial decrease of heat losses.

Control system

To control the system is automated by a programmed PLC. It is programmed in a way that it operates autonomously. But in case of a system error it is possible to remotely overrule the automated operations and start or shut down subsystems manually.

Conclusion

The results of this project are an Energy Evaluation Model and a Concept solution for sustainable energy supply for remote buildings in the Kvarken archipelago. The evaluation model is a useful tool for engineers for the estimation of the electricity and heat needs of a building. The concept solution is divided into four sizes. Two generic sizes, sized smaller than 5 kW and five to 10 kW. Moreover, two specific solutions are produced, one concept for Mickelsörarna and another concept for Valsörarna.

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List of Units

°C	Celsius Degree
g	Gram
m ²	Square meter
m³	Cubic meter
m/s	Meter per second
I	Liter
%	Percentage
W	Watts
kW	Kilowatts
kWh	Kilowatts hour
Т	Temperature
J	Joules

List of Abbreviations

1 ST	First
2 ND	Second
AC	Alternate Current
ASHP	Air Surface Heat Pump
Avg	Average
СНР	Combined Heat and Power
Co LTD	Limited Company
CO ₂	Carbone Dioxide
COP	Coefficient of Performance
DC	Direct Current
E	East
EDLC	Electric Double Layer Capacitor
Elec.	Electricity
EPS	European Project Semester
ERV	Energy Recovery Ventilation
G.K.	Green Kingdom
GSHP	Ground Source Heat Pump
H ₂	Hydrogen
HP	Heat Pump
HRV	Heat Recovery Ventilation
i.e.	For Example
MS	Microsoft
MW	Megawatts
Ν	North
NE	Northeast
NRCan	Natural Resources Canada ??
ND	No Date
NW	Northwest
0.Y.	Osakeyhtiö, Limited Company
Р	Pressure
PEM	Polymer Electrolyte Membrane
S	South
SE	Southeast
STP	Standard Temperature and Pressure
SW	Southwest
SWHP	Surface Water Heat Pump
TINOX	Titanium Nitride Oxide
UNESCO	United Nations Educational, Scientific and Cultural Organization
U.S.	United States
VDC	Volts Direct Current
W	West

Preface

European Project Semester (EPS)

The European Project Semester is a program offered by ten European universities in eight countries throughout Europe. The purpose is to prepare engineering students with all the necessary skills to face the challenges of today's world economy. The students meet in international teams of 2-10 students from these different countries to work on their dedicated projects. International student teams are composed to match the students' specializations and capabilities as well as to develop their inter-cultural communication and teamwork skills. (Yrkeshögskolan Novia, 2012)

Six students from Spain, the Netherlands, Belgium, China and Finland compose the EPS spring 2012 - team. All students have different degrees as mechanical engineering, electrical engineering, product development and human technology engineering.

Members



Name: Oriol Ala Puig Country: Spain University: Universitat de Lleida

Mechanical Engineering

Name: Hui Liang Country: China University: Novia University

Electrical Engineering

Name: Rida Lahmaidi Country: Spain University: Universitat Politècnica de Catalunya

Mechanical Engineering

Name: Christophe Hopchet Country: Belgium University: Artesis Hogeschool Antwerpen

Product Development

Name: Tim Eebes Country: the Netherlands University: Hanzehogeschool Groningen

Human Technology Engineering

Name: Simon Lillqvist Country: Finland University: Novia University

Electrical Engineering

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1 Introduction

1.1 Task

The Kvarken Archipelago near Vasa is a group of islands located on the western shore of the Gulf of Bothnia. It became Finland's first and only natural UNESCO world heritage site in July 2007. (Kvarken World Heritage, n.d.)It is an internationally valuable natural area with many important habitats and endangered species. The area is characterized by its small size and its biological and geomorphological diversity (Anders Enetjärn, Lise-Lotte Molander, n.d.). Some of the islands in the archipelago contain buildings. These buildings are old coastguard stations that nowadays serve as nature stations. More information about the buildings is given in chapter 3.1 on Mickelsörarna and in 3.2 on Valsörarna. The nature stations are only used in the summer for recreational and tourism purposes. In the winter the concrete buildings suffer from the cold and humidity. They need to be heated to prevent decay.

This European Project Semester (EPS) comprises two tasks. The first task was to make an evaluation model for the energy demands for remote places like Mickelsörarna and Valsörarna. The model may contain technical terms, so people that are comfortable with these terms can use the model. This part of the project will continue during the summer for other islands and harbor stations. The usability of this evaluation model is an important factor in this assignment. The second task was to research and develop a sustainable solution for the energy demands on Mickelsörarna, Valsörarna and a generic solution for other buildings in the archipelago.

The EPS project group was encouraged by the management to look for an innovative solution, to think outside the box. Cost would not be a big issue, if the solution was found satisfactory.

1.2 Goals

The goal of this EPS is to generate a sustainable and mostly autonomous solution for buildings in the Kvarken archipelago. This means that it can last for many years with little maintenance needed. Another important aspect is the whole system being environmentally friendly, without any harmful emissions to nature. The new solution should not only be sustainable and autonomous, but also an investment to lower the costs in a time range of 20 years.

1.3 Tools

To help this EPS group to succeed, tools are given by Novia University of Applied Sciences, or arranged by project members themselves. The most used tools are:

- Lectures
- Tritonia Academic Library
- Internet
- Weekly meetings
- MS Project
- Experts from commercial companies

In the first phase of this project, **lectures** were given about different subjects in relation to the project. The purpose of these lectures was to get to know each other and learning the expertise needed for this project.

The project started with two introduction days to get to know the campus, the city and the group members. The lectures started with 'team building and cultural difference' sessions, given by Mr Roger Nylund. The same week, Christian Nelson gave the group a guided tour of the university library Tritonia, as well as the digital resource database. Furthermore, there was a lecture called 'Project work, my way' by Mr Jan Teir. Mr Jan Teir is the owner of this project. His experience and expertise in project work is a guidance in this assignment. He also gave a lesson on 'MS Project', to use the software as a planning tool. Next to that there were 'energy solutions' lectures by Mr Ronnie Sundsten and Brush-up English by Ms Ulla-Maj Söderback.

The **library** was used to gather knowledge and information about energy solutions, electricity needs, off grid examples and fuel cell basics. The main source in this project is however the **Internet**. Information given by questionable internet sources are avoided or double-checked.

An important tool during this project were the **Project Meetings**. Every week there was at least one project meeting with the project owner and the project manager. During these meetings the students had to present their research, decisions and accomplishments of the previous week. The role of chairman and secretary were rotary, so that every team member had the opportunity to learn from this experience. During the project meetings the project manager and project owner gave feedback and guidance to the team.

At the end of the engineering phase (phase II) specific answers about the final solutions were desired. To get these answers experts were contacted and asked if they were willing to cooperate. Some experts were lecturers; some **experts** were from **commercial companies**.

1.4 Limitations

This project aimed for a sustainable energy solution for remote places in the Kvarken archipelago in Finland. The weather conditions in the archipelago and the location of these islands are two factors that have made the result of this project relevant in only this region. The purpose of the project is to generate a plausible specific and generic solution for buildings in the archipelago, taking these two factors into account. The reasons why the solutions have been chosen will be substantiated and the used technology will be explained in an understandable way, without that previous knowledge of the matter being necessary.

2 Project

2.1 Work Methodology

The European project semester in Vasa offered by Novia University of Applied Sciences is focused on energy and environment. EPS projects may also contain other essential elements, such as communication, management, planning, European law, innovation, marketing and language. (European Project Semester, KL, 15-12-2011). Novia's EPS website states: *'The EPS-program is crafted to address the design requirements of the degree and prepare engineering students with all the necessary skills to face the challenges of today's world economy.'* (Yrkeshögskolan Novia, 2012)

To successfully complete this project, it is split up in three phases. The three phases are:

- Phase I: Brainstorming and Idea Generation
- Phase II: Engineering
- Phase III: Documentation

Every phase has a different organization. The roles of Project Leader and Project Administrator change every phase and are decided in Phase I. **Phase I** consists of brainstorming and idea generation. The goals are made clear, concept ideas are generated, and the choices made are backed up with facts.

Phase II is the engineering phase. This is the phase where calculations and concept drawings are made about the final decisions in the project

Last phase is **phase III**, the documentation phase. In this phase the final report is written and the project presentation is made. At the end of the phase the final report is handed in and an oral presentation of the project is given.

Communication

A weekly project meeting is carried out in order to communicate the progress of this project to the project owner and project manager. During these meetings the Project leader hands in a written Weekly Status Report, which contains the following information:

- Summary of tasks completed in previous week
- Summary of tasks scheduled for completion next week
- Summary of issue status and resolutions
- Summary of the project status
- Summary of time usage (per student) including tasks
- All above-mentioned summaries are made with the same template

Desk research

Desk research is the main research method used in this project, with the Internet as primary information source. The project started without any previous research. During all phases, desk research has been used to obtain knowledge and data about e.g. similar projects. It started in phase I with looking at the current state of technology. In phase II it was used to find the right equipment, suppliers but also additional knowledge. In phase III it was used to gather and apply knowledge about writing regulations for scientific reports.

2.2 Logo

To enhance the group coherence and presentation, the EPS team created a logo (*Figure 1*). The logo has been used on every presentation material used outside the team.



Figure 1: EPS Spring 2012 team logo

The logo is a green leaf with the name of the project team, eps2012s. The name is just an abbreviation of European Project Semester 2012 Spring. The team adopted this name and used it throughout the rest of the project. The leaf and the green represent the sustainability factor in this project.

2.3 Ekenäs Fair

Phase I was ended with a presentation of the concept on the Novia environmental fair in Ekenäs. The Environmental Fair 2012 is an event jointly organized by Novia University of Applied Sciences, the City of Raseborg and Ekenäs Energy Company (Yrkeshögskolan Novia, 2012). The main goal of the fair was to learn how to prepare and present this project at a fair. To accomplish this goal two posters, a business card and a presentation were produced. (Appendix 01: Ekenäs Fair Posters and Appendix 02: Business Card)

2.4 Website

To inform anyone interested in this project, there is a website. <u>http://eps2012s.novia.fi</u>. This address is mentioned on the business cards. The website contains information about the project, the team members and the archipelago. It will be kept up to date, until the end of the project, to inform the interested persons about the latest developments in this EPS project.

2.5 Visit to Mickelsörarna

This EPS started on February 1, 2012. At that time the archipelago was covered in ice. Due to the ice conditions in the archipelago it was impossible to go safely to the islands. This meant that the team had to work with the information provided by Novia and pictures of the buildings on the islands. In April, after the melting of the ice the team visited Mickelsörarna. The main purpose of the visit was to extract data and to get an impression of the state of the building. The building was closely inspected, and the amount of electricity for the appliances was checked. Besides that the team had the opportunity to exchange thoughts with the responsible engineers of the building on Mickelsörarna (*Figure 2*).



Figure 2: Visit to Mickelsörarna

3 Energy demands

In this chapter, the use of the energy evaluation model is explained, and the results of this model applied on the nature stations of Mickelsörarna and Valsörarna are shown.

3.1 Energy evaluation model

As mentioned in chapter 1.1, the energy evaluation model is the second aspect of the project.

The result is a spreadsheet made for calculating the electricity needs as well as the heat losses for a building. The evaluation is suitable for off-grid, remote buildings, as they can be found on e.g. Mickelsörarna and Valsörarna. To use it correctly, both models include an instruction manual *(Appendix 03: Instruction Manual Electricity Evaluation).*

3.1.1 Electric Evaluation

The electric evaluation consists of two parts. The AC (Alternate Current)(*Figure 3*) and the DC (Direct Current)(*Figure 4*). The person who uses the evaluation model needs to know the power consumption of all the appliances that are or will be used in the building, the quantity and the amount of hours that the appliances run in summer and in winter.

By filling in the white cells with this data the model calculates the average and peak electricity consumption, depending on the season. If an appliance is not used during wintertime, change the quantity to 0. This means that the model will not take the appliance into account in the calculations about total energy.

ALTERNATE	SUMMER				WINTER						
Appliance Name	Power (W)	Quantity Summer	Total (W)	Hrs/day	W/hrs per day	AVG Load	Quantity Winter	Total (W)	Hrs/day	W/hrs per o	AVG Load
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0.00	0.00		0		0.00	0.00

Figure 3: Electric Evaluation Model-AC load

DIRECT CU	RRENT ((DC)		SUMMER			WINTER					
Appliance Name	Power (W)	Quantity Summer	Total (W)	Hrs/day	W/hrs per day	AVG Load	Quantity Winter	Total (W)	Hrs/day	W/hrs per day	AVG Load	
			0		0,00	0,00		0		0,00	0,00	
			0		0,00	0,00		0		0,00	0,00	
			0		0,00	0,00		0		0,00	0,00	
			0		0,00	0,00		0		0,00	0,00	
			0		0,00	0,00		0		0,00	0,00	
			0		0,00	0,00		0		0,00	0,00	
			0		0,00	0,00		0		0,00	0,00	
			0		0,00	0,00		0		0,00	0,00	
			0		0,00	0,00		0		0,00	0,00	
			0		0,00	0,00		0		0,00	0,00	
			0		0.00	0.00		0		0.00	0.00	

Figure 4: Electric Evaluation Model-DC load



Figure 5: Electric Evaluation Model-Total electricity needs

At the bottom of the Electric Evaluation sheet there is a summary of the Electricity needs (*Figure 5*). The average consumption and the peak consumption are calculated. These numbers are needed in further calculations of the size of the installation for the power supply.

Due to the unreliable power supply, generated by sustainable energy sources (e.g. wind energy), a secondary power supply is needed. It is used to cover the electricity needs when the energy generated by the primary system is not enough (e.g. not enough wind when using a wind turbine). This model calculates the size of a battery bank and the size of a hydrogen tank for a fuel cell backup system (*Figure 6*).

Voltage of DC System in V	48	v
Number of Days Backup storage is required	72	Hours
Efficiency of Back up System in %	80%	%
Maximum Discharge in %	70%	%
Est. Size of Energy Storage ¹ (Batttery Bank)	0,00	Ah
Pressure in Bars	30	Bar
Energy Density of H ₂ (STP)	3,5	STP
Efficiency	40%	%
Total Back up Energy	0,00	KWhrs
Total energy from H ₂	0.00	KWhrs
H ₂ needs	0.00	Liters STP
	0,00	Enters STP
Est. Size of Hydrogen Storage Tank ²	0.00	Liters

Figure 6: Electric Evaluation Model-Secondary power supply

3.1.2 Heating Evaluation

The total heat loss is calculated by the sum of the losses due to transmission and ventilation. Both are given after the input of building and environment information such as wall area and components (windows and doors), construction materials, used ventilation system and temperature difference.

It will be used to establish a correct idea of the energy consumption of the investigated building. The use of the model starts with filling in the data for the losses due to ventilation (*Figure 7*):

- **Outside** minimum average temperature [in Celsius degrees].
- Ground minimum average temperature (approximate) [in Celsius degrees].
- Inside objective temperature [in Celsius degrees].
- Approximate **Volume** of building [in m³].
- Air changes per hour (see table on the bottom).
- Air Heat Recovery System Efficiency. If there is none, write 0 (zero) [in %].



Figure 7: Heating Evaluation Model-Heat loss due to ventilation

The following step is the surfaces of the building. Starting with the wall area and materials (*Figure 8*). It is possible to choose up to four different materials per wall. Then the size of the windows and doors are filled in. This results in the calculation of thermal transmittance of the building.

Element	Projected view areas (m ²)	roof pitch correction factor (30º inclination)	Materials	Thermal Resistance R (m ² ·K/W)	Thermal Transmittance U (W/m ² ·K)	HEAT LOSS due to TRANSMISSION H _{TI} =Area _i •U ₁ ·Δ _{Temp}
Outside Wall 1						
			Wall material	#N/A	#N/A	#51/6
			Choose wall	#N/A	#N/A	#19/8
			material from	#N/A		
windows & doors in wall 1			input R			
Outside Wall 2				#N/A		
				#N/A	#11/0	#51/6
				#N/A	#N/A	# N/A
				#N/A		
windows & doors in wall 3						

Figure 8: Heating Evaluation Model-Heat loss due to transmission

The model creates a summary with the total heat loss of the building in Watts(Figure 9).

OBJECTIVE TEMPERATURE INSIDE (%C)	APROXIMATE VOLUME of BUILDING (m ³)	TOTAL HEAT LOSS
GROUND TEMPERATURE (PC)	AIR CHANGES per hour *(see table below) (defect 1)	#N/A
MINIMUM AVERAGE TEMPERATURE (%C)	Air Heat recovery system Efficiency (%)	Watts

Figure 9: Heating Evaluation Model-Heat loss summary

3.1.3 Summary

The last sheet of the Evaluation Model is a summary of the complete evaluation (Figure 10).

RESULTS Summary	PROJECT		0	
ELECTRICITY	SUMMER		WINTER	
Average Energy Consumption	0,00 kWh		0,00	kWh
Power Peak (100%)	0,00	kW	0,00	kW
Size of Energy Storage	0,00	Ah]	
72 hours 48 Volts			-	
Volume of H2 Storage	0,00	liter]	
30 bar				
HEATING				
Max. Heat Loss	#N/A	kW]	
Building Transmittance	#N/A	W/m2.K]	
Inside Temp Ground Temp. Outisde Min. Temp.) °C		

Figure 10: Evaluation Model-Summary

These numbers can be used for the design of the building and for the design of the power and heating systems.

The developed EEM comes with this report. Because it is a digital working model, it is added to this report. It is to be found on a CD that is located is the back of this report. The CD contains the EEM as well as the manual how to use the model

3.2 Mickelsörarna

Mickelsörarna is a group of islands in the Kvarken archipelago. They are located at the northeast corner of Kvarken and the group comprises almost 300 islands. Relatively deep waters surround the large and small-forested islands. (Enetjärn & Molander, 2002)

On one of the islands called Kummelskäret, there is a former coastguard station which nowadays serves as a nature station (*Figure 11*) This building needs a sustainable electricity and heat generating solution. The station contains a café, which is open for tourists during the summer. Furthermore, there is a mobile phone base station, which has a constant electricity demand throughout the year.



The owner of the building is the Finnish forest administration (Forststyrelsen/Metsähallitus).

Figure 11: Nature station on Mickelsörarna (ÖFPL/Göran Strömfors, n.d.)

To dimension the power and heating systems, the demands needed to be known. The best option would have been to apply the Energy Evaluation Model as shown in chapter 3.1. However, most of the building construction data required to apply the Model was not available. Therefore, the calculations were based on the existing data from different sources, provided by the Project Managing Director.

Data:

- Document1: Tilastoja Suomen ilmastosta 1981-2010
- Data extracted from it can be found in the appendices (Appendix 07: Weather Data).
- Document2: Osa 1- sähkölaite ja kulutuskartoitus
- Document3: Osa 2- 97-07 kulut
- Document4: Osa 4-5 Optimaalinen energiantuotantosunnitelma

Mr. Kari Hallantie provided other basic information and blueprints, from the Finnish Forest Administration (Forststyrelsen/Metsähallitus) (*Appendix 05: Blueprints Valsörarna*).

Below follows a summary of the data gathered from the aforementioned sources:

- Main building (the one that has to be heated):
 - Located in the highest point of the island
 - Built in 1987
 - 2 stories + guard tower + basement
 - 689 m² useful surface
 - 1994 m³ volume
- Electricity production:
 - 2 Diesel generators (75kW and 50kW) (Ford 2525E and Ford 2526E)
 - Wind turbine (3.2 kW) (Whisper 500)
 - Solar panels (2.1 kW) (Neste Oy NP100G/24)
- Thermal energy production:
 - Oil fired water heater (Riello 3062 428TI) (glycol instead of water)
 - Diesel generators exhaust gas waste heat collectors for hot water
- Operation 1997 to 2008
 - Fuel consumption 76250 l
 - 57850 I to electrical energy production
 - Max. 578500 kWh of energy, efficiency of about 30% => about 173000 kWh
 - 18400 I to heating
 - Heating only used during the winter
 - Generators oversized => running 10-30% load
 - Mobile phone station 35 kWh/day, 12780 kWh/year, 2000 to 2007, total 102200 kWh
 - Cafeteria open during summer months

3.2.1 Heating

Due to the lack of specific data of the heat needs for the main building in Mickelsörarna, the heat needs had to be calculated in some other way. Among the data available there was the fuel consumption for heating purposes and the amount of fuel used to generate electricity, which are detailed in *Table 1*. However, the fact that the exhaust heat from the diesel generators for electricity production was recovered made the calculations more imprecise because of the assumptions made.

	Fuel Burning	Waste from Elec. Production	
Fuel consumed / 11 years (I)	18400	57850	
Fuel consumed / year (I)	1673	5259	
Efficiency	*90%	*40%	
Energy density(kWh/ I)	9,8		
Months ON	6	12	
Energy (kwh)	14753 20616		
Total energy / year	35369 kWh		
Power (kW)	3,37	2,35	
Total power 5,7 kW			

Table 1: Heat needs on Mickelsörarna

*assumptions

Assumptions

There is a level of uncertainty with the results obtained due to some assumptions that had to be made. These are the assumptions:

- Efficiency of the fuel oil burners: 90%
- Efficiency of the exhaust heat recovery system: 40%
- Energy density of Diesel fuel: 9,8 kWh/l (it differs depending on the fuel)

Reliable historic climate information was necessary in order to estimate when and how much heating was needed. Taking the weather data into account, one can see how the temperature drops below 10^o from October until May, and below 0^oC from December to March (*Table 2 and Figure 12*).

Month	Avg. temp (ºC)	Heating usage
Sep	10,6	Off
Oct	5,8	50%
Nov	1,2	50%
Dec	-2	100%
Jan	-4,5	100%
Feb	-5,5	100%
Mar	-3,1	100%
Apr	1	50%
Мау	6	50%
Jun	11,1	Off

Table 2: Average temperatures during the winter and usage of heating estimation



Figure 12: Average temperatures from September to June

After the calculations the conclusion reached was that the amount of **Power needed for heating Mickelsörarna**'s building is about **5.7 kW**, From that the used energy in a year becomes **35369 kWh of Energy**.

3.2.2 Electricity

The electricity has been produced combining the following systems:

- 2 Diesel generators (75kW and 50kW) (Ford 2525E and Ford 2526E)
- Wind turbine (3.2 kW) (Whisper 500)
- Solar panels (2.1 kW) (Neste Oy NP100G/24)

The electrical energy is necessary to feed the heating system, the electrical appliances in the building and the Mobile Phone Station. During the summer months a cafeteria/restaurant service operates in the building *(Table 3).*

	Time	kWh / day	Power	kWh / year		Yearly electricity consumption
Mobile Phone Station	all year	35	1,5	12775	12775	
Restaurant	5 months	45	1,9	6843	7605	20470 kWh
Stand by	7 months	4	0,17	852	7655	

Table 3: Electricity consumption detailed

Electrical needs for heating

This table shows the consumption for the past years. The solution concept presented in this report uses a heat pump to provide the heating energy needed in the building. The mentioned heat pump needs electricity to run and produce the 5.7 kW of heat needed. The COP used for the calculations was 3. Therefore, to achieve those 5.7 kW of heat power, the electrical need is 5.7/3. That means less than 2 kW of electricity. Water pumps are also part of the system. Taking that into account and to make up for the assumptions made during the heat needs calculations, the electricity need for the heating system used will be 3.3 kW.

Electrical needs for the building

The Energy Evaluation Model developed by the EPS team was applied to calculate the electrical needs of the building in Mickelsörarna. This is the result obtained (*Table 4*).

Table 4: Electricity needs for Mickelsörarna obtained with the energy evaluation model

TOTAL ELECTRICITY NEEDS		ER	WINTER	
AVERAGE AC CONSUMPTION	3,35	KWhrs/h	5,00	KWhrs/h
PEAK AC CONSUMPTION	13,29	KW	5,38	KW
Inverter ((requires 10% Energy DC/AC))	14,62	KW		

The detailed spreadsheet with the appliances can be found in *Appendix 08: Mickelsörarna Electricity Needs.*

Conclusion

As a conclusion the average Power Demand for Mickelsörarna is about **3.3 kW in the summer** (Cafeteria/Restaurant + Mobile Phone Station), and **4.4 kW in the winter** (Heating + Mobile Phone Station). Especially in summer, when the power demand is less steady, the need to cover the possible demand peaks must be taken into account.

3.3 Valsörarna

Valsörarna is another part of the archipelago, located west from Mickelsörarna and more central in the Kvarken area. The islands are known for their important bird sanctuary and the 36-metre tall iron lighthouse (*Figure 13*). The lighthouse was designed in 1886 in Paris by the same firm that later built the Eiffel Tower. On Äbbskär, an island of Valsörarna, there is a coast guard station that also needs a sustainable energy solution. (Enetjärn & Molander, 2002)

The owner of this building is different than the owner of Mickelsörarna, namely the Finnish State properties. (Senatfastigheter).



Figure 13: Lighthouse on Valsörarna (ÖFPL/Göran Strömfors, n.d.)

For Valsörarna no information on electricity consumption or heat needs was available. The study case had to be based on blueprints and documents of the building for the calculation of the heat losses due to construction. Those documents were requested of the Finnish State Property (Senatfastigheter), the owner of the building on Valsörarna.

These are the documents on which the calculations were based:

-Blueprints (Copies of these can be found in Appendix 05: Blueprints Valsörarna.

- LEIKKAUS
 CUT VIEW
- JULKISIVUJA: LOUNAASEEN, LUOTEESEEN
- JULKISIVUJA: KAAKKOON, KOILLISEEN
- KELLARI
- 1. KERROS
- 2. KERROS
- ULLAKKO

FACADES: SW, NW FACEDES: SE, NE BASEMENT 1ST FLOOR 2ND FLOOR ATTIC (guard tower)

-Documents:

RAKENNUSSELITYS Mv-asema Valassaaret, ARKKITEHTIOTOIMISTO SALMINEN JA VÄRÄLÄ OY,

Helsinki 1982. (BUILDING DESCRIPTION Nature Station Valsörana)

Below there is a summary of the data obtained from the aforementioned sources:

-Main building (the one that has to be heated):

- Built in 1982
- 2 stories + guard tower + basement
- Around 760 m² surface
- Around 1864 m³ volume

-Different floor/wall/roof types transmittances:

- Floor AP1: k=0,33 W/m²^oC (outer region), k=0,33 W/m²^oC (inner region)
- Floor VP1: k=0,42 W/m²⁰C
- Floor VP2: k=0,42 W/m²^oC
- Floor VP4: k=0,24 W/m²^oC
- Roof YP1: k=0,17 W/m²⁰C
- Wall US1: k=0,43 W/m²⁰C
- Wall US1: k=0,43 W/m²^oC
- Wall US2: k=0,35 W/m² C
- Wall US3: k=0,23 W/m²^oC
- Wall US4: k=0,24 W/m² C

-Windows are a 3-glass with air gap + 2-glass with air gap.

-Average minimum temperature in the coldest months is -20ºC.

3.3.1 Heating

The determination of the heat needs was made by calculating the heat losses of the building, according to its construction, building material, weather data, etc. the Energy Evaluation Model was used.

The areas of every wall, floor, ceiling, windows and doors had to be calculated as a first step to be able to apply the Energy Evaluation Model. Then there was data available for most surfaces and the calculation could be done (*Table 5*).

T inside	5	°C		
T outside	-20	°C		
T ground	0	°C		
HEAT LOSS THROUGH				
Walls	2490,5125	Watts		
Windows	3744,290865	Watts		
Doors	625	Watts		
Basement	1446,51	Watts		
Roof	1118,9375	Watts		
Ventilation	618,75	Watts		
TOTAL HEAT LOSS	10044	Watts		

Table 5: Building heat loss calculation using energy evaluation model summary

The complete calculation sheet can be found in Appendix 10: Valsörarna Heat Needs.

Some assumptions had to be made to estimate the transmittance of surfaces of which data was missing. Conservative criteria were used to decide which values would be used for the calculations. These assumptions are listed below.

Assumptions

- Surfaces and volumes were calculated from the blueprints
- k of walls with no data: 0,25 W/m²^oC
- k for all roof types will be the same
- 1 complete air change per day with an air heat recovery efficiency of 50%

The calculated result is the **Heat Loss**. The heat need for the VALSÖRARNA's Nature Station Building is therefore: **10kW**.

3.3.2 Electricity

The electrical energy is necessary to feed the heating system and the electrical appliances in the building. There was no data used about the way electricity has been produced earlier.

Electrical needs for heating

As calculated in chapter 3.3.1, the heat loss of the building is about 10 kW in the coldest days. Calculating with a COP of 3 for the heat pump, we can obtain that the electrical power need of the heating system is around 3,3kW.

Electrical needs for the building

The Energy Evaluation Model developed by the EPS team was applied to calculate the electrical needs of the building on Valsörarna. In this building there is no cafeteria/restaurant, so the energy need during the summer period is very low. Even the average need is low, around 1.5 kW is used for the building appliances. The electricity demand of the building will come in peaks.

This is the result obtained (Table 6):

TOTAL ELECTRICITY NEEDS	SUMM	ER	WINTER	WINTER	
AVERAGE AC CONSUMPTION	0,50	KWh/h	4,37	KWh/h	
PEAK AC CONSUMPTION	9,20	KW	17,20	KW	
Inverter ((requires 10% Energy (DC/AC))	10,12	KW			

The complete calculation sheet can be found in Appendix 09: Valsörarna Electricity Needs.

Conclusion

As a conclusion, the average Power Demand for Valsörarna is about **0,5 kW in summer**, and **5 kW in winter** (mainly for the heating system). The need to cover the possible demand peaks in summer, when there might be visitors in the building, must be taken into account.
4 Different concepts

At the end of the brainstorming phase (phase I) three different concepts were generated. One of these had to be chosen for further investigation and calculation in this project. The requirements were set at the beginning of this project. It had to be autonomous, sustainable, low-maintenance and last for approximately 20 years. The three different concepts are:

- Storage by Hydrogen
- Storage by Super Capacitors
- Waste to energy

4.1 Storage by Hydrogen



Figure 14: Different concepts - Stored by hydrogen

Figure 14 shows the first concept. This concept uses a wind and solar power as main power system, which, when the production exceeds the demand, converts water into hydrogen, and when the production is not big enough for the demand, that hydrogen is converted again into water and electricity. This hybrid system is chosen because of the favorable weather data and the fact that one of the islands already owns a wind turbine and solar panels. The main challenge in this project is the storage of electricity. In this concept the excess energy from the main power source is conducted to an electrolyzer that converts purified water into hydrogen and oxygen. The hydrogen is stored in a tank. When there is not enough power available from the main power system, the hydrogen is released into a fuel cell, which converts the hydrogen into electricity. The heat is supplied by a heat pump. This is known technology in Finland. The heat extracted by the collecting pipes can come from earth, water or air. This has to be investigated in the next stage.

Advantages of using hydrogen as a fuel for energy storage are:

- 2.5 to 3 times more efficient than gasoline.
- No CO₂ emissions.
- It is not toxic.
- In case it leaks, it dissipates very easily in the air.
- It can be stored under pressure, reducing storage space.

The disadvantages are:

- The total system has a low efficiency (up to 60% electricity, up to 85% with heat recovery)
- Young technology
- Expensive

This concept was forwarded to the Engineering Phase for further investigation and calculations.

4.2 Storage by Super Batteries



Figure 15: Different concepts - Stored by super batteries

The second concept is similar to the concept 'Storage by Hydrogen'. The difference is the method of storing excess electricity (*Figure 15*). Instead of using hydrogen and a fuel cell or traditional batteries, the excess electricity in this concept, is stored by super batteries. A super battery is a conventional battery in conjunction with a super capacitor. A super capacitor (also known as EDLC, electric double layer capacitor) differs from a regular capacitor in that it has a very high capacitance.

Advantages of using super batteries are:

- Uninterrupted Power Supply
- Extends the lifetime of a battery (up to 4 times)
- 25% of the cost of a NiMH battery

Disadvantages are:

- High self-discharge rate
- Requires sophisticated control and switching equipment
- Spark hazard when shorted

This concept was forwarded as well. More research was needed to choose between Storage by Hydrogen and Storage by Super Batteries.

4.3 Waste to energy



Figure 16: Different concepts- Waste to energy

The final concept creates electricity and heat out of waste. *Figure 16* is a schematic view of this concept. Raw materials as biomass, sewage, municipal waste and green waste are gathered and placed in a Combined Heat Power unit (CHP unit). In this concept waste is burned, and the energy obtained from the waste is converted into electricity and heat. There is an island in Denmark (Bornholm) that is partially powered by a waste to energy concept. The major difference is that Bornholm is inhabited and the islands in the archipelago are not.

Advantages of Waste to Energy are:

- Reduction of Landfill Disposal
- Greenhouse Gas Emissions reduction
- The fuel obtained cheaply
- Biogas can be stored

The disadvantages of this system are:

- The islands are uninhabited
- No one to operate the plant all year round
- No production of waste all round the year, as it is uninhabited

Due to these substantial disadvantages, the Waste to Energy concept was discarded.

4.4 Other discarded possibilities

The presence of water around the islands makes the possibility to gain energy from water movement an interesting subject for research. The kinetic energy created by waves, tide or currents can be converted into electric power. The use of compressed air is also a way to store energy. In this chapter we discuss these different possibilities with the reasons why they were discarded.

4.4.1 Wave energy

Waves are created by the wind blowing over the sea surface. The water absorbs the energy from the wind and starts to move in phase. Waves are thus basically an direct effect of wind energy. A system to exploit this wave energy is called Wave Energy Converter (WEC). A WEC installation has two major disadvantages when compared to wind turbines, it is twice as expensive and it needs constant maintenance.

In the Gulf of Bothnia, the average wave size is small. When the wind speeds are highest, it is winter and the sea is frozen, so no energy can be gained (WindFinder, 2012).

4.4.2 Tidal energy

Tidal energy, or tidal power, is a form of hydropower that converts the energy of tides in electricity. Tides are more predictable than wave, wind and solar energy.

The Gulf of Bothnia has no tides or significant currents, which is the reason why current and tidal power is discarded as a usable system. Furthermore, this system involves high costs, limited suitable building sites for barrages and it affects the costal environment (darvill.clara.net, 27-02-2012).

4.4.3 Storage

Hydroelectric energy

This method stores energy in form of water. The water is pumped to a higher located water storage, and released through turbines to generate electricity during periods of high electrical demand. This system responds quickly and accurately to the increasing or decreasing demand. The hydroelectric system is discarded because of the absence of height differences in the archipelago, and the small usable space (darvill.clara.net, 2012).

Compressing air in a cave

Energy can also be stored by compressing air. When the electrical demand is low, the excess electricity is used to compress air. The compressed air is stored in natural underground caves. The efficiency of this system is over 75% (REUK, 2012). However, this system is discarded because of the absence of caves in the archipelago.

Underwater air bags:

Another solution is to store compressed air in flexible underwater accumulators. 'The weight of the water keeps the air at pressure. Stored air is then released and converted back to electricity when required.' (Tomorrow is greener, n.d.). This system is discarded because it requires a water depth of 600 meter and the water depth around the archipelago is too shallow.

Conclusion

A summary of the forwarded solutions to the engineering phase is made below in *Table 7*. The main power system uses wind and solar power. The heat will be provided by a heat pump and excess energy will be stored as hydrogen or by using super batteries.

Table 7: Summary of the forwarded solutions

PRIMARY POWER SOURCE	SECONDARY POWER SOURCE + STORAGE	HEAT SOURCE	
Wind Turbing	Batteries	Air	
	Super Batteries	Seawater	
Photovoltaic Panel		Ground	
Wind Turbing + Photovoltaic	Electrolyzer + H ₂ Storage + Fuel		
	cell	Exhaust Heat Recovery	
		Energy Recovery Ventilation	

The following steps in the engineering phase were:

- How much energy is needed?
- How much energy is there in the wind?
- How much energy is there in the sun?
- How is the energy going to be stored? (Hydrogen or batteries)
- How much energy does need to be stored?

5 Systems

In this chapter the different systems that were forwarded from phase I are investigated and described. Based on this information the final decisions about the systems are made. The used systems are divided into Electricity, Heating and Ventilation, and a Control and Monitoring system.

5.1 Electricity

The electricity demand will be covered at all times by using a combination of different systems. These are a Primary System, which will be responsible for the main power load, a Secondary System, which will store energy and convert it into electricity when the Primary System can't fulfill the demand, and finally there will be an emergency back-up system, in case there is a malfunction in the aforementioned systems.

5.1.1 Primary system

The primary system is responsible for obtaining the necessary amount of energy to cover the electricity needs of the islands. During the whole year the needs differ from island to island, depending on the amount of electrical appliances in the building and the presence of an eventual base station and radar station. The different available sources of renewable energy and the ways to use these sources to generate electricity are researched and described in this chapter.

Available energy sources

The main source of renewable energy in the archipelago is wind. This is because the wind is available the whole year round. In *Table 8* the exact information about average wind speed and directions can be found.

Table 8: Wind speed

						Tuu	lien jak	autum	uinen – N	Vind o	listribu	tion						
Kk		N	N	Æ	1	E	s	E	s		ST	N	W	7	N	N	Tyyni Calm	Ka Mean
Month	m/s	%	m/s	%	m/s	%	m/s	%	m/s	%	m/s	%	m/s	%	m/s	%		
3003	Ν	IUSTA	SAARI	VALA	SSAAF	RET												
4	0.0	10	7.4	0	c 0		47	4.4	0	10	7.6	45	74	10	7.0	10	4	0.0
1	8,0	13	7,4	8	0,0	8	4,1	14	0,9	19	C, 1	CI 4C	7,1	13	1,3	10	1	0,8
2	7,9	10	1,4	11	5,2	8	4,2	12	0,8	22	6,9	10	0,5	12	0,5	1	1	0,2
3	7,5	12	0,0	11	4,6	8	4,3	9	6,8	21	5,7	15	6,0	10	5,9	1	1	5,7
4	7,1	12	6,5	17	4,3	8	3,8	6	6,2	25	5,2	14	5,4	10	5,5	6	1	5,3
5	5,9	12	6,0	19	4,0	8	3,6	3	6,0	24	5,0	17	5,0	10	4,9	7	0	4,9
6	5,7	13	5,6	19	3,8	9	3,0	4	6,0	21	4.8	16	4.7	10	4.9	8	1	4,7
7	5.7	11	5.5	16	3.8	8	3.3	6	5.4	22	4.7	17	4.8	10	5.0	8	1	4.6
8	6,6	12	6,2	16	4,6	9	3,6	8	5,2	19	4,9	17	5,4	10	5,8	8	1	5,1
9	7.4	11	6.7	11	5.0	8	3.8	10	5.7	20	5.9	16	6.8	13	7.2	11	1	5,9
10	8.8	12	7.5	7	6.8	7	4.7	13	6.9	20	7.0	18	7.5	13	7.8	9	1	7.0
11	8.9	12	8.6	7	7.2	8	5.0	16	6.8	18	8.0	16	7.6	12	7.7	10	1	7.4
12	8,7	12	9,1	7	6,8	7	4,6	15	7,0	18	7,6	15	7,6	14	8,0	12	0	7,2
	7,3	12	6,9	12	5,2	8	4,1	10	6,3	21	6,1	16	6,2	11	6,4	8	1	5,9
able cou		innich	Motor	rolog	ical In	.+:++.	2012	`										

Table source: (Finnish Meteorological Institute, 2012)

This data is collected by a weather station on Valsörarna, located 30 km southwest of Mickelsörarna. The complete document is *Appendix 07: Weather Data*. Based on the aforementioned data, wind is a considerable power source in this area. The use of a wind turbine will make maximum advantage of this available source.

A second energy source is the sun. There is a difference in the amount of sun power available in winter and summer. Below is a *Table 9* with the average sun isolation along the year.

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec
Insolation, kWh/m²/day	0.13	0.70	1.81	3.69	5.28	5.91	5.43	4.03	2.42	0.99	0.29	0.05
Clearness, 0 - 1	0.25	0.39	0.43	0.51	0.53	0.52	0.51	0.48	0.45	0.37	0.34	0.20
Temperature, °C	-7.01	-7.9	-4.3	0.71	7.16	12.37	15.42	14.39	10.09	5.09	-0.3	-4.1

Table 9: Solar insolation

Table source: (Chinci, 2011)

The table above shows the solar insolation. Insolation is the amount of radiation that strikes the surface of the earth in a given time. With the insolation the amount of energy that can be obtained from the sun is calculated. In this area, the solar energy is only usable during the spring and summer months, the rest of the year the amount of energy that can be obtained is insignificant. This means that depending on solar energy as a single energy source is not reliable. Another factor to take into account is snow. It is likely that during the winter the solar panels will be covered with snow. However, like mentioned before, during the winter months the solar energy that can be obtained is insignificant.

Based on the available sources, a study of the viability of different systems or a combination of systems that could ensure a big enough power availability around the year was required.

Wind turbines

Wind turbines can be divided into two big groups: vertical and horizontal wind turbines. The vertical turbine's axis is located perpendicularly to the wind direction, they don't need to be oriented to face the wind. They are less efficient, because of their configuration. The wind that makes them rotate also slows them down when it pushes the backside of the blades. The horizontal turbine's axis works parallel to the wind, therefore it needs to be continuously oriented to face the wind. These wind turbine's are more efficient because none of the blades are moving against the wind (*Figure 17*) Each of those groups can be divided according to the different blade shapes or configurations possible for them.



Figure 17: Vertical and Horizontal wind turbines configurations (Gregor Hopkins, 2007)

The two systems operate differently, but their functioning principle is the same: to extract part of the energy in the wind to create electricity. That energy is found in the moving air molecules. Since they have a mass and a speed, they contain kinetic energy.

Kinetic Energy in 1m³ of air:

Kinetic Energy: $E_{k} = \frac{1}{2} \text{ m} \cdot \text{v}^{2}$

- Energy E[Joules]
- Mass m[kg]
- Velocity v[m/s]
- Mass of air at sea level is around 1,23 kg/m³

Then, the power available from each square meter of that moving air is:

Wind Power: $P_w = \frac{1}{2}$ density $\cdot v^3$

- Power P_w [W/m²]
- Density [kg/m³]
- Velocity v[m/s]

For the most common type of wind turbines (horizontal axis) the area swept by the blades is:

Swept area: $\mathbf{A} = \pi \cdot R^2$

- Swept area A[m²]
- Radius R[m]

Therefore, the available power in the wind that passes through a wind turbine is:

Power Available: $P_A = \frac{1}{2} \cdot 1,23 \cdot v^3 \cdot \pi \cdot R^2$

- P_A [W]
- 1,23 kg/m³ (Air density)
- Velocity v[m/s] (Wind Speed)
- Blade Radius R[m]

To collect that energy from wind, wind turbines convert the kinetic energy into mechanic energy, by turning a shaft, which is connected to a rotor. That rotor is turning inside a stator, and there the mechanical energy is converted to electric energy. The amount of energy in the wind after the turbine is lower, since it loses speed. That energy differential is what has been transformed into electricity by the wind turbine (*Figure 18*). Typically wind turbines are able to use about 30-40% of that available power from the wind and can be scaled to obtain from a few hundred watts up to several megawatts of clean power.



Figure 18: Wind energy diagram (LP ELECTRIC SRL, 2004)

Solar Panels

There are basically two ways of getting energy from the sun: collecting thermal energy and converting electromagnetic radiation into electricity by photovoltaic solar panels or solar cells.

The thermal energy collector may not be a suitable option for this project, due to the location of the buildings. This far north, the amount of thermal energy that can be collected from the sun is too small. Moreover, during the winter months the snow may be a problem for the system. More information about solar heat collectors can be found in chapter 5.2.2.

A solar cell converts sun radiation into electricity using the photovoltaic effect (Hertz effect). This is the emission of electrons from matter. When this matter gets hit by electromagnetic radiation, this radiation will be absorbed. Since the solar radiation that reaches the Earth is quite stable (changes slowly), those electrons emitted become an electric flow or current. One solar cell can only produce a very small amount power, therefore cells are mounted in panels, forming arrays, to reach a reasonable power output (*Figure 19*). The efficiency of the solar panels to exploit the solar isolation is around 15 %.



Figure 19: Solar cell panels functioning (Advanced Energy Industries, Inc, 2012) (Greenteam Renewables Ltd, 2012)

Around 175 PW (PetaWatts, $1PW = 10^{15}W$) of solar radiation in all its forms (insolation) arrive to the earth in the upper atmosphere. One third or less of that amount gets reflected back to space. The rest is absorbed by clouds, oceans and landmasses. The principle of solar panels is to collect part of that power and convert it into a usable form of energy (*Figure 19*).

"Solar Radiation Reaching the Earth

The intensity of the solar radiation reaching us is about 1369 watts per square metre $[W/m^2]$. This is known as the Solar Constant. It is important to understand that it is not the intensity per square metre of the Earth's surface but per square metre on a sphere with the radius of 149,596.000 km and with the Sun at its centre.

The total solar radiation intercepted by the Earth is the Solar Constant multiplied by the cross section area of the Earth. If we now divide the calculated number by the surface area of the Earth, we shall find how much solar radiation is received, on average, by a square metre of the Earth's surface. Thus, the average solar radiation S per square metre of the Earth's surface is:

Sun Power = $S \cdot \pi . r^2 / 4\pi r^2 = 1369 / 4 \approx 342 W / m^2$

where S in the Solar Constant in W/m^2 and r is the Earth's radius.

Solar Radiation Reaching the Earth Surface

However, our calculations are not yet finished because we have not yet considered the influence of the Earth's atmosphere. The value we have calculated is for the average solar radiation intensity at the outer regions of the Earth's atmosphere. What we want to know is how much of this radiation reaches the earth surface where we are

The atmosphere absorbs about 68 W/m^2 and reflects 77 W/m^2 (Wallace and Hobbs 1977). The radiation reaching the Earth's surface is therefore on average **198** W/m^2 , i.e. 58% of the radiation intercepted by the Earth." (Dr. Ron Nielsen, 2005)



Figure 20: Average Insolation 1991-1993 (Matthias Loster, 2010)



Figure 21: Sun Power reaching the Earth (William B. Stine, Michael Geyer, 2001)

Conclusion

Out of the gathered information the conclusion can be made that the use of a hybrid system for the main power system would be the best option. Hybrid means that two different energy sources will complement each other to cover the energy needs throughout the year. In chapter 4 all the studied options to obtain energy are discarded, except Wind and Sun. Solar energy can cover a bigger demand during the summer and wind energy can cover a bigger demand during the winter.

5.1.2 Secondary system

In a stand-alone, off the grid system electrical power availability represents a great challenge. One of the main goals of the EPS project was to obtain that power somehow sustainably. There are ways to produce power using clean renewable sources. In this case the ones chosen were Wind and Sun. The availability of these sources is intrinsically uncertain. Therefore, a way to store the excess electrical energy produced while the demand is smaller than the production was necessary. The main problem is that electrical energy cannot be stored as itself. It has to be transformed in some other form of energy that can be stored. These are the different forms of energy and some examples of how they could be stored, as well as their main advantages and disadvantages (*Table 10*).

Form	Storage	Advantages	Disadvantages
Electrical energy	Not possible	-	-
Kinetic energy	Increasing the speed of a flywheel	Very high efficiency	Technically complicated, several moving parts, high maintenance
Potential (gravitational) energy	Pumping up water into a tank or damp	High efficiency	Big space and construction needed
Thermal energy	Heating up a fluid or gas in an isolated tank	High efficiency	Big losses, limited amount storable
Chemical energy	Converting a substance into another one, that when converted back would release energy	Reliable, low maintenance, big storage capacity and easily expandable	Low efficiency, young technology, cost

Table 10: Comparison of forms of energy and their storage

For the small size of the installations in the Kvarken Archipelago, as well as the automated nature of the solution searched, it became clear that the best way to store that electricity would be as chemical energy.

Different systems studied

Three ways to store energy in a chemical form were studied:

- Super Batteries
- Batteries
- Hydrogen (Electrolyzer + Tank + Fuel Cell)

Super Batteries

A super capacitor is known as a double layer capacitor. They store electricity by physically separating positive and negative charges—unlike batteries, which do so chemically. It polarizes two conducting plates who are made of a porous material to store energy electro statically. Due to this material the plates have bigger surface and thus an increased storage capacity. This mechanism is highly reversible, and allows the ultra capacitor to be charged and discharged hundreds of thousands of times (supercapacitors.org, n.d.).

Super capacitors in a hybrid system are usually referred to as super batteries or ultra batteries. In this case the super capacitor is used as a buffer between device and battery. The super capacitor is able to handle short interruptions; the battery is needed to store enough energy for longer interruptions.

Table 11 Below shows the advantages and limitations of super capacitors.

	Virtually unlimited cycle life; can be cycled millions of time			
High specific power; low resistance enables high load current				
Advantages	Charges in seconds; no end-of-charge termination required			
	Simple charging; draws only what it needs; not subject to overcharge			
	Safe; forgiving if abused			
	Excellent low-temperature charge and discharge performance			
	Low specific energy; holds a fraction of a regular battery			
	Linear discharge voltage prevents using the full energy spectrum			
Disadvantages	High self-discharge; higher than most batteries			
	Low cell voltage; requires serial connections with voltage balancing			
	High cost per watt			

Table 11: Advantages and disadvantages of super capacitors

Table Source: (Isidor Buchmann, 2012)

As the above table shows, a super capacitor has very high self-discharge rate. The stored energy of a super capacitor decreases from 100 to 50 percent in 30 to 40 days. A nickel-based battery self-discharges 10 to 15 percent per month (Isidor Buchmann, 2012).

The conjunction between a super capacitor and a battery is promising. At this moment, however, the state of technology of super capacitors is at the top of innovation. The ultra capacitors are currently not available for this project.

Batteries

Many different types of batteries exist. The main concept by which they work is always the same. When a device is connected to a battery, a reaction occurs that produces electrical energy. This is known as an electrochemical reaction. The Italian physicist Count Alessandro Volta first discovered this process in 1799 when he created a simple battery from metal plates and brine-soaked cardboard or paper (Marshall Brain, Charles W. Bryant and Clint Pumphrey, 2012).

Advantages:

- Know technology
- Easily sizable
- Low cost recharging

Disadvantages:

- No complete discharge, usually 70% discharge rate
- Costs, over 20 years, at least 2 battery banks are needed
- Takes time to charge
- Die suddenly, no smart chips inside batteries

(George Loker, n.d.)

Rechargeable batteries are used as a backup source for energy. On Mickelsörarna there is an existing battery bank. The lifetime of a battery is about 7 years. A goal of this project was to create a solution that, after the investment, has low costs for 20 years. Replacing the battery bank every seven years means that this goal is not reached. Comparing costs shows that, due to the purchase of multiple battery banks, storing by hydrogen is economically more reasonable.

Hydrogen

Compressed hydrogen is another way to store chemical energy, as it can be scaled up or down to suit the needs. Hydrogen is generated from water. As a fuel it is 2.5 to 3 times more efficient than fossil fuels. There are no CO_2 emissions if natural sources are used to produce that hydrogen. It is safe because it is not toxic and since it is the lightest element existing, it dissipates very easily in the air. Hydrogen can be stored under high pressure, making the space required for the tanks smaller.

Comparison and Conclusion

Technical Comparison	Battery	Fuel cell	
Capacity	depends on the number of	depends on the size of the fuel	
Capacity	batteries	storage	
Efficiency	higher	low (40%-50%)	
Fuel storage location	inside	outside	
programmable control	no	yes	
lifespan	<10 years	>10 years	
Maintenance cost	low	low	
20+ years cost	high	low	
Installation	2251/	complex (combine electrolyzer	
	easy	and H_2 storage)	
Ambient temperature range	need air conditioning	wide	
Environmental impact	has pollution	almost zero emission	

Table 12:	Comparison o	of fuel	cell and	battery
-----------	--------------	---------	----------	---------

As Table 12 shows, batteries have a shorter lifespan than fuel cells. For example, 'lead-acid batteries have a lifetime shorter than ten years even in optimal conditions (ambient temperature 20° C or less), due to their inherent chemical instability' (Anders Ocklind, 2005). This is because that both the capacity and reliability of the battery usually degrade with time. The capacity of the battery reduces very fast at low temperature. This is a disadvantage in cold climates as it is in Finland. Normally, before the battery dies it should be replaced, just in case some problems should occur. Furthermore, replacing the battery also increases the total cost. (Anders Ocklind, 2005)

'Hydrogen fuel cell systems are best suited for the applications in which the power need is low (<10 kW) and the energy needs are high (>10 kWh)' (Anders Ocklind, 2005), as shown in Figure 22 below.



Figure 22: Solutions for different power and energy needs applications (Anders Ocklind, 2005)

For the buildings on the islands that the EPS project team are working with, the power needs are normally below 6 kW and the energy needs are far bigger than 10 kWh, therefore the best solution for the project is to use hydrogen fuel cell systems.

HYDROGEN system choice

The reasons to use hydrogen as an energy storage system are the following:

- It is generated from water + electricity, no other chemical products supply needed.
- 2.5 to 3 times more efficient than gasoline.
- No CO₂ emissions if generated with renewable power sources.
- It is not toxic.
- In case it leaks, it dissipates very easily in the air.
- It can be stored under pressure, reducing storage space.

There are three main stages to be studied in the process: Production, Storage and Utilization. Another aspect that will also be considered is the Reutilization of Water from the Fuel Cell. Lastly, the safety issues must be considered during the entire process.

The aforementioned stages are analyzed, described and calculated in Appendix 11: there are also the tables with the main characteristics of the different technologies for every system, with their advantages, disadvantages and reasons for choosing or discarding them.

Hydrogen production: PROTON EXCHANGE MEMBRANE (PEM) ELECTROLYZER

The choice made was to get the hydrogen from **Splitting Water Molecules**, particularly with a **Polymer Electrolyte Membrane** (or PEM) Electrolyzer, since it was the system that suited better the requirements and needs for the project. The main characteristics of PEM electrolyzes and the reasons why it is the best option are:

- There is no liquid electrolyte, simplifies the design significantly
- The PEMs can operate with a high pressure output
- They use an acid polymer membrane
- They are suitable for both mobile and stationary applications
- Large turn-down ratio, meaning that they can operate efficiently off their peak power zone
- They are safer than other kinds of electrolyzers thanks to the lack of hazardous chemicals
- The PEMs can be built in a small size because of the high pressure that can be reached
- They offer quite high efficiencies for CHP (combined heat and power)

Next is a brief explanation of the system inside a PEM electrolyzer (more detailed in Appendix 11: Secondary Power System).

Polymer electrolyte membrane (PEM) electrolysis

The REDOX reaction that takes place in the electrolysor:

Anode (oxidation):	$2 H_2 O \rightarrow O_2 + 4 H^+ + 4e^-$	E ^o _{ox} = -1.23 V
Cathode (reduction):	$2 \text{ H}^{+} + 2 \text{e}^{-} \rightarrow \text{H}_{2}$	$E_{red}^{o} = 0.00 V$

The negative voltage in the oxidation of the anode means that the reaction needs energy to take place.

This could be simplified by combining the two previous reactions:

Overall reaction: $2 H_2O(I) + Electricity (1.23 V) --> 2 H_2(g) + O_2(g)$

Even though it is the best choice for the circumstances, there are some challenges that should be mentioned: PEM technology is not as a mature technology as alkaline, due to the relatively high cost, the low capacity (enough for the project needs), an efficiency up to 60% for electricity, and up to 85% for CPH. In the past few years PEM technology and performance have improved significantly.

The electrolyzer model that has been chosen of the different situations is shown in *Table 13* below. More information about this electrolyzer can be found in Appendix 17: Electrolyzer Datasheet

Table 13: PEM electrolyzer choice for each application

Application	Choice
Smaller needs concept (<=3.5 kW)	
Bigger needs conpcet (3.5 to 5 kW)	Acta Enormy AES200*
Mickelsörarna (4.4 kW)	Acta Energy AES200
Valsörarna (5kW)	

*This device is suitable for all the different systems.

Hydrogen storage: Pressurized Gas Steel Tank

The most adequate hydrogen storage system for the characteristics of this project (remote isolated location, automated, easy maintenance, safety, available space) is to use a pressurized steel tank containing gaseous hydrogen at no more than 30 bar.

The reasons for making that choice are the following:

- It is cheaper than other similar solutions, like composite tanks.
- It can operate at cold temperatures (liquid storage requires cryogenic temperatures).
- It doesn't require a heat input to extract the hydrogen (solid storage does).
- It is safe. In case of leakages, gaseous hydrogen dissipates easily in the air.

To calculate the size of the tank needed for every one of the four different specific applications of the concept some different factors were studied. These factors are:

-	Electrolyzer Output and efficiency	depend on model
-	Fuel Cell Input and efficiency	depend on model
-	Energy availability from hydrogen time	1week
-	Power density of hydrogen under STP	3.2 - 3.5 Wh/l

Calculations can be found in Appendix 11: Secondary Power System

Therefore the adequate tank for each one of the applications should be as follows (Table 14):µ

Table 14: Pressurised gas steel tank choice for each application

Application	H ₂ tank
Smaller needs concept (<=3.5 kW)	< 15000 liters H ₂ @ 30bar,25 ^o C
Bigger needs concept (3.5 to 5 kW)	15000-20000 liters H ₂ @ 30bar,25 ^o C
Mickelsörarna (4.4 kW)	20000 liters H ₂ @ 30bar,25 °C
Valsörarna (5kW)	20000 liters H ₂ @ 30bar,25 °C

Hydrogen usage: PROTON EXCHANGE MEMBRANE (PEM) FUEL CELL

Fuel cells are the best way to convert the chemical energy stored in hydrogen into electricity. Particularly Polymer Membrane Fuel Cells are the most suitable choice for the project because of their characteristics:

Following, there is a brief explanation of the system inside a PEM fuel cell (more detailed in Appendix 11: Secondary Power System).

Proton Exchange Membrane (PEM) FUEL CELL

PEMs use a solid polymer as an electrolyte and carbon electrodes containing platinum catalysts that are very sensitive to CO. They are suitable for light-duty applications (cars, buildings). It makes them an ideal replacement for rechargeable batteries (*Figure 23 and Table 15*). More characteristics and advantages of these PEM fuel cells are listed below:

- High power density (W/m³)
- Safer due to lack of hazardous chemicals
- Low temperature operation which results in a quick start-up (short warp-up time)
- Few or no moving parts at all
- Low weight and volume
- Maintenance becomes a less important issue
- They are scalable, from a small number of cells to a large stack depending on the need
- Efficiencies from 35 to 60 for electricity
- Efficiencies up to 85 or 90% for CHP (combined heat and power)
- PEM fuel cells have zero emissions
- No combustion process means no NOx or SOx
- Very low noise and vibrations, if any



Figure 23: Fuel cell operation diagram (U.S. DEPARTMENT OF ENERGY, Energy Efficiency & Renewable Energy (EERE), 2011)

The chemical reaction that takes place inside a fuel cell is the same as in the electrolyzer, but naturally it is reversed, with an input of H2 and O2 and an output of H2O and electricity (and heat):

Anode:	$H_2> 2H^+ + 2e^-$	$E^{o}=0V$
Cathode:	$\frac{1}{2}$ O ₂ + 2H ⁺ + 2e ⁻ > H ₂ O	E ^o = 1.23V
Overall reaction:	$H_2 + \frac{1}{2}O_2> H_2O$	E ^o = 1.23V

Table 15: PEM fuel cells characteristics

Fuel Cell Type	Common Electrolyte	Operating Temperature	Typical Stack Size	Efficiency	Applications	Advantages	Disadvantages
Polymer Electrolyte Membrane (PEM)	Perfluoro sulfonic acid	50-100°C 122-212° typically 80°C	< 1kW-100kW	60% transpor- tation 35% stationary	 Backup power Portable power Distributed generation Transporation Specialty vehicles 	 Solid electrolyte re- duces corrosion & electrolyte management problems Low temperature Quick start-up 	Expensive catalysts Sensitive to fuel impurities Low temperature waste heat

Table Source: (U.S. DEPARTMENT OF ENERGY, Energy Efficiency & Renewable Energy (EERE), 2011)

According to the electricity needs calculated for each of the applications, the choices for the Fuel Cell that fit each of the concepts best are found below in *Table 16*. More information about these fuel cells can be found in Appendix 18,19 and 20

Table 16: PEM fuel cell choice for each application

Application	Туре
Smaller needs concept (<=3.5 kW)	ReliOn T-2000 [®] 4kW Outdoor Configuration
Bigger needs conpcet (3.5 to 5 kW)	Dantherm DBX5000
Mickelsörarna (4.4 kW)	Dantherm DBX5000
Valsörarna (5kW)	Dantherm DBX5000

Water reutilization

The electrolyzer needs to be fed water with a high grade of purity. Therefore, this water must be brought to the islands and stored waiting to be used to produce hydrogen. This hydrogen will be converted into water vapor in the fuel cell, while electricity is generated. Then the vapor will be conducted through a condenser where it will condense into pure water. This water will be reutilized by the electrolyzer. In this way the system is closed, and the need for a constant input of pure water for the electrolyzer can be neglected. Nevertheless, the system will never be 100% closed, as there will always be a certain level of water loss. For that reason the size of this pure water storage should be enough to fill the hydrogen tank, plus a little bigger, to fulfill the assumed losses (*Figure 24*).



Figure 24: Water reutilization diagram

Hydrogen safety and regulations

'It is important to understand the properties of hydrogen and safety requirements for storage, refueling and use of hydrogen. Hydrogen displays extreme characteristics, either very low (density ignition energy at stoichiometric ratio) or very high (buoyancy in air, diffusion coefficient in air, flammability range, velocity of laminar burning at stoichiometric ratio, heat of combustion and detonation sensitivity) as compared to other fuels (methane, propane, gasoline vapour).' Minna Nissilä (Minna Nissilä, 2011).

Therefore, there is a risk with hydrogen unless some safety measures are taken into account, due to the aforementioned characteristics and some others, such as:

- Colourless and odourless
- One can asphyxiate by breathing hydrogen
- Very wide flammability limits in air mixtures (4 to 75%)
- Low ignition energy
- Almost invisible flame
- Small molecular size promotes leaks and diffusion
- Highly reactive with oxygen and other oxidizers
- High flame temperature
- Negative Joule-Thomson coefficient: leaking gas warms and may spontaneously ignite
- Can diffuse into or react with certain metals

Hydrogen is the smallest element that exists. This makes leakages easy, even through the solid metal walls of a tank, which can also react with H_2 . The reaction causes changes in the mechanical properties of the metal. Hydrogen will ignite in air with a concentration three times smaller than it would take to ignite gasoline (4 to 75%). It burns in with a pale blue flame, almost invisible, thus you could discover a fire by walking into it. It can accumulate in closed spaces, but easily disperses in open spaces.

For those reasons, special care must be taken with hydrogen systems.

Regulations

These are the regulations to follow when installing and operating hydrogen systems (electrolyzers, storage and fuel cells, and transportation):

CHEMICAL SAFETY Chemicals Act (744/1989) Act on the safety of the handling of dangerous chemicals and explosives (390/2005) Decree on the industrial handling and storage of dangerous chemicals (59/1999)

ATEX

European Directive 99/92/EC (also known as the 'ATEX Workplace Directive') In Finland: Government decree on prevention of the danger caused by explosive atmospheres (576/2003) European Directive 94/9/EC (also known as 'the ATEX Equipment Directive') In Finland: Decree on equipment and protective systems intended for use in potentially explosive atmospheres (917/1996) Decision of Ministry of trade and industry on equipment and protective systems intended for use

Decision of Ministry of trade and industry on equipment and protective systems intended for use in potentially explosive atmospheres (918/1996)

PRESSURE EQUIPMENT

Pressure equipment Act (869/1999) Decision of Ministry of Trade and Industry on pressure equipment safety (953/1999)

ENVIRONMENTAL PORTECTION Environmental protection Act (86/2000)

RESCUE

Rescue Act (468/2003) and the Government Decree on rescue (787/2003) If still up to date

LAND USE AND BUILDING Land use and building Act (132/1999) and the Land use and building decree (895/1999)

MACHINERY AND TECHNICAL DEVICES

Act on the conformity of certain technical devices to relevant requirements (1016/2004) Government decree on machinery safety (400/2008)

Conclusion

For the secondary power system, the most suitable solution that fitted the needs of the project is to use a hydrogen system. It will consist of a combination of a PEM electrolyzer, a compressed gas steel tank to store it and a PEM fuel cell and a water-cooling and reutilization system.

Once each one of the cases has been studied, the conclusion reached is that for every one of them there has to be some variation as regards the choice of the products (except for the electrolyzer, the model chosen suits all the studied cases).

Hydrogen is a potentially dangerous material, if not processed and stored correctly. Therefore a list of directives and regulations must be followed to ensure the safety functioning of the system once it is operating in its location.

5.1.3 Back-up Generator

The islands in the archipelago are uninhabited during the winter season. Because of the ice conditions the islands in the archipelago are inaccessible during the winter. Due to the inaccessibility, maintenance of buildings and equipment during the winter season is impossible. The minimum required temperature inside the buildings is five degrees Celsius. To ensure this demand, there is a back-up generator in this concept, besides a primary and secondary energy system,

In case of a complete system failure, the generator will start automatically ensuring that the heat needs are satisfied. If the fuel cell is turned off for any reason, there is the possibility to start the generator manually.

If necessary, the possibility exists to use the generator to cover the biggest peaks in the energy demand. However, it is impossible to automate the system in a way that the generator starts when there is a power peak. The startup time of the generator is too slow. If there is an expected high power peak, the generator has to be started manually.

Based on this information the requirements are set. The generator needs be to established:

- Biofuel engine
- Remotely started
- Hydrocarbon free emissions
- External Fuel Tank Option
- Security monitoring
- Integration in renewable systems



Figure 25: Backup generator-TELGENCO 48-5 (Telgenco, 2012)

The Quiet48-5 (48 V DC, 5kW, *Figure 25*) made by Telgenco is designed for remote rural areas and integration in a renewable energy solution. Key benefits of the generator chosen for this concept are:

- 100% Biofuel engine option
- Automated Remote Control
- Full engine and monitoring control
- Clean 48 VDC Power output
- Environmentally inert materials
- Environment Operating Temperature: -40 / +55 Celsius
- Optional external tank connection

The specifications of this backup generator suit the needs of this project. Telgenco is a company that is committed to protecting the environment. This generator is made of environmental inert materials and designed to be almost completely recycled at the end of its life. (Telgenco, 2012).

The bio fuel engine option allows the system to be used as a totally hydrocarbon free renewable energy exchange with consequent environmental benefits. In this project where the main goal was to make a sustainable solution, this aspect is essential. The energy needs for the heating in this project are approximately 3,5 kW. This is during the coldest weeks when the temperature drops to -27° Celsius. Telgenco makes two generators in this line, a 2 kW and a 5 kW. As stated above, the 2 kW is not sufficient for the heating needs all year round. This 5 kW generator generates a 48 V DC current. Most equipment used in the buildings are 230 V AC, therefore it needs to be inverted to 230 V AC. An inverter is already scheduled in this concept; the generator needs to be wired to the inverter as well.

5.2 Heating

Heating is an important aspect for the maintenance of concrete buildings in winter. The buildings need a constant inside temperature of 5°C. Without this heat, the lifetime of a concrete building will shorten drastically.

The research done during the project shows that the use of a heat pump is the most suitable system to provide the necessary heat.

5.2.1 Heat pump

The function of a heat pump (*Figure 26*) is based on the phase changes of a refrigerant. Thermal energy is absorbed from a primary source (ground, water or air) and transported by a pipe loop to the evaporator of the heat pump. The first heat exchange happens in the evaporator as the liquid refrigerant turns in to vapor. The temperature and pressure of the vapor increase by using a compressor. In the condenser of the heat pump, the vapor turns into a liquid again. The released energy is transferred into the output heating circuit. An expansion valve is placed after the condenser causing the refrigerant to cool.



Figure 26: Working of a Heat Pump (Radiant Floor, 2011) / Modified

СОР

COP, the abbreviation of Coefficient Of Performance, is the ratio between the quantity of heat delivered and the energy required by the heat pump. This is used to compare the efficiency of heat pumps. The COP is dependent on the difference between the source temperature and the desired output temperature. The bigger the difference, the smaller the COP.

An electric resistance heater has a COP of 1. Therefore an electric resistance has an efficiency of 100%. Usually, a heat pump has a COP between 2 and 5. A COP of 3 means that the system has an efficiency of 300%. The COP can be calculated with the equation below (Figure 27):.

 $COP = \frac{Quantity \ of \ Heat \ Delivered}{Energy \ Required \ by \ the \ Heat \ Pump}$

Figure 27: The equation of COP calculation

Heat source

A heat pump (HP) can get its heat from three main sources:

- Ground (GSHP)
 - Closed/Open loop
 - Surface Water (WSHP)
 - Closed/Open loop
- Air (ASHP)

The **ground source heat pump** collects the solar energy that is absorbed and stored in the ground during the summer. Around 46% of the Sun's energy is absorbed by the earth (Figure 28).



Figure 28: Distribution of solar energy (NRCan, 2002)

Because of the high heat storage capacity and a low thermal conductivity of the earth, the heat that is stored in the summer provides a free renewable source of energy that can easily provide enough energy to heat-up a building in the winter. Another characteristic of the ground is that a few meters of surface soil insulate the earth below. This means that at a certain depth you will get a constant ground temperature throughout the whole year. (NRCan, 2002)

There are two ways (*Figure 29 and Figure 30*) to collect the heat from the ground, a closed loop and an open loop piping system. The heat collecting pipes of the closed loop system can be buried horizontally or vertically depending on the available space and climate conditions. Brine with anti-freeze properties is used in the pipes.



Figure 29: Horizontal GSHP (Thermia Partners Oy, n.d.)



Figure 30: Vertical GSHP (Thermia Partners Oy, n.d.)

The open loop piping system uses a well to pump up ground water to the heat exchanger in the HP *(Figure 31).* The water is then returned to a separate injection well. Corrosion and the possibility of fouling decrease of the water flow are the major issues in this system.



Figure 31: Open loop GSHP (Industrial boilers, 2011)

A HP can also use **surface water** as heat source (*Figure 32*). Surface water can be a pond, a lake, a river or the sea. Similar to GSHPs, the difference can be made between closed loop and open loop systems. The pipes of the close loop system are immersed in the water body and are kept on the bottom with weight.



Figure 32: Closed loop WSHP (Thermia Partners Oy, n.d.)

The open loop system withdraws water from the water supply by using a pump. The water flows through the heat exchanger in the HP (*Figure 33*) and then flows back in the water body. For this system the use of a water body with a certain amount of current is preferable.



Figure 33: Open loop WSHP (Southern Company, 2012)

The **air source** heat pump (ASHP, *Figure 34*) uses the air as a heat source. The pump aspires the outside air and conducts it to the heat exchanger in the HP. In the heat exchanger the heat gets transferred to air or water which is used to heat the building.



Figure 34: Air source heat pump (Thermia Partners Oy, n.d.)

5.2.2 Heating trade-off

In the trade-off a comparison is made between all the possible heating solutions based on 8 different criteria (Appendix 12: Heating & Ventilation Trade-off). A score between 1 and 5 is given for each criteria of each solution (a 5 is the best score). This score is multiplied by a factor of importance. The factor, also between 1 and 5, marks the importance of the criteria in relation to the solutions. In the end the scores of each criteria are added to a total. This gives a good general view of the qualities of every solution.

The results of this trade-off are shown in the figure below (Figure 35).

	Ground heat	Closed loop		97	1
	Ground near	Open loop		80	4
I last summer		Bottom	Closed loop	76	5
Heat pumps	(sea)Water heat		Open loop	82	3
		Under sediment		89	2
		67	7		
Solar collector	Eva	70	6		

Figure 35: Comparison of all the possible heating solutions

Evacuated Heat Tubes

The trade-off contains solar collectors as one solution. This has nothing to do with heat pumps, but the use of evacuated heat tubes is a solution worth looking at. It is a very efficient way to collect solar radiation to heat up water. The collector is made of a vacuum tube with a heat pipe in the middle. This heat pipe transports the collected heat to a heat exchanger that is in contact with the water storage tank.

With the Titanium – Nitride – Oxide (TINOX) absorber coating, 98% of the incoming solar radiation can be absorbed, and temperatures above 230°C are achievable (Dr. F. Mahjouri, 2004).

Unfortunately, due to the big amount of snow in winter, the pipes get covered and stop working. Removing the snow should be done delicate because the pipes are very fragile. Replacing the pipes each time one breaks can get very expensive.

Conclusion

The first two options that are discarded are evacuated tubes and the 'under sediment' heat pump. The evacuated tubes because of the reasons mentioned in the paragraph before. The sediment heat pump is discarded for the reason that there are too many rocks in the sediment, which would make it very difficult and expensive to bury the pipes in the sediment.

Furthermore, air source heat pumps are not efficient in cold climates such as in Finland. Mitsubishi came up with a hyper heating pump system that uses a so called 'H2i[®] technology'. These cold climate heat pumps can work in temperatures that reach -30°C with a COP of 1.5 to 3.0. The reason for discarding this option is the reliability. The heat pump contains a lot of moving parts. That increases the risk of failure and shortens the lifetime of the system. An example of this system can be found in Appendix 12.

Three possible heating options remain: the ground source heat pump and the open and the closed loop water-sea heat pump. The advantages and disadvantages of these three systems are summarized below.
Option I: Ground source heat pump



Figure 36: GSHP

Table 17: Advantage and disadvantage of ground source heat pump

Advantages	Disadvantages
Sustainable	
No maintenance	
 No moving parts 	
 Buried in the ground 	
Reliable	Expensive
 No seasonal influence 	• System
 Stable input temperature 	 Transportation to the island
Efficient	Borehole drilling
 High heat profit because of the high 	
input temperature	
Not visible from the outside	
Longest lifetime	

Option II: Closed loop water source heat pump



Figure 37: Closed loop WSHP

The advantages and disadvantages of option II is made in comparison with option III in the *Table* 18.

below

Option III: Open loop water source heat pump



Figure 38: Open loop WSHP

Table 18: Advantages and disadvantages of closed loop and open loop WSHP

Option II: Closed loop WSHP		Option III: Open loop WSHP			
Advantages	Disadvantages	Advantages	Disadvantages		
Use of a anti-freeze brine • Higher heat profit	Less efficient • One heat	Cheap • Less pipes	Corrosion by seawater • Adequate		
	exchange more		equipment Expensive 		
No maintenance	Possible damage by storm	Efficient One heat exchange less 	No anti-freeze brine • Outgoing water can freeze • Small heat profit		
	More expensive • Longer pipes	Small risk of damage	Maintenance of filters		
	Higher electricity consumption • Bigger pumps				

5.2.3 Ground source heat pump

Further investigation of the three possible options that are left by using the trade-off, the decision is made to use the vertical loop GSHP.

Heat input

Brine in the vertical collecting pipes is absorbing the heat. The pipes are placed in boreholes with a depth of 100 to 200m. At that depth the ground has a stable temperature. The figure below shows that in Finland the ground temperature stabilizes to 6°C at a depth of 7m (*Figure 39*).



Figure 39: Ground temperature versus depth (R.Lemmelä, Y.Sucksdorff, u.d.)

This ground property makes the GSHP more efficient than any other conventional heating technologies.

Heat output

After the fluid in the pipe loop has collected the ground heat, it exchanges its heat with the heat pump. The pump increases the heat (the working of a heat pump can be read in paragraph '4.2.1 Heat pump') and delivers it to a hot water accumulator. From there, the hot water can be used in a radiator or floor heating system.

5.3 Ventilation

Ventilation is the process of renewing the used inside air of a room by fresh outside air. It helps to control the humidity, reduce indoor pollutants and odors, avoid moisture and assures a healthy and comfortable living environment. High humidity levels can even lead to structural damage of the building. Ventilation can happen naturally or mechanically. (U.S. Department of Energy, 2011)

5.3.1 Natural vs. Mechanical

Natural ventilation

Natural ventilation is the penetration of outside air into a building by natural forces. These forces can be wind or pressure difference and are dependent on the weather conditions. The fresh air can penetrate through cracks, small holes, and openings around doors or simply by opening a window. It is an uncontrolled passive process that requires neither energy nor maintenance. In cold climate regions, this kind of ventilation is not recommended because of the higher heat losses. (U.S. Department of Energy, 2011)

Mechanical ventilation

Mechanical ventilation or whole-house ventilation forces the air to move inside and/or outside a building. A uniform air movement is created by electrically driven fans and conducted by pipes. In this way, the air exchange is able to happen deeper in a building and is easier to control. (U.S. Department of Energy, 2011)

There are three types of mechanical ventilation systems:

- Exhaust ventilation
- Supply ventilation
- Balanced ventilation
 - Energy Recovery Ventilation (ERV)
 - Heat Recovery Ventilation (HRV)

Exhaust ventilation systems work by extracting the inside air of a room, to create a lower pressure than outside the building (*Figure 40*). This pressure difference induces an incoming fresh airflow that penetrates the room through leakage in the building shell or/and, more preferable, through intentional vents. Adjustable, passive vents are placed in windows or walls to prioritize the incoming flow rather than rely on the building leakage. If the pressure difference created by the ventilation system is too small, the passive vents won't work efficiently. (U.S. Department of Energy, 2011)

'Exhaust ventilation systems are most applicable in cold climates. In climates with warm humid summers, depressurization can draw moist air into building wall cavities, where it may condense and cause moisture damage.' (U.S. Department of Energy, 2011)



Figure 40: Exhaust Ventilation (U.S. Department of Energy, 2011)

Supply ventilation works in the opposite way than the exhaust ventilation by creating a higher pressure inside the building (*Figure 41*). This pressure forces a fresh supply of air into the room and drives exhaust air outside the building. Supply ventilation allows the incoming air to be filtered and dehumidified. In cold climates however, the system has the potential to create moisture problems due to condensation on the cold exterior walls. This can induce mold, mildew, and decay. (U.S. Department of Energy, 2011)



Figure 41: Supply Ventilation (U.S. Department of Energy, 2011)

In a **Balanced ventilation** system, the incoming and outgoing airflow is equal or balanced (Figure 42). It is a combined exhaust and supply ventilation system, thus it requires the double amount of fans, ducts and pipes. This system can be equipped with an energy or heat recovery system. Based on the recovery system you can divide balanced ventilation into two groups: Energy Recovery Ventilation (ERV) and Heat Recovery Ventilation (HRV). The difference between ERV and HRV is the way the heat exchanger works. The heat exchanger in an ERV-system transfers a certain amount of water vapor along with the heat, while an HRV-system only transfers heat. (U.S. Department of Energy, 2011)



Figure 42: Balanced Ventilation (U.S. Department of Energy, 2011)

Conclusion

Both exhaust and supply ventilation systems don't recuperate the heat from the outgoing airflow or remove the moist from the incoming air before it enters the building. This results in higher heating costs compared to a balanced ventilation system equipped with an energy recovery system. Most of the energy recovery systems have an efficiency of 70 to 80%, or even more in climates with extreme winters. (U.S. Department of Energy, 2011)

5.3.2 Ventilation trade-off

In the trade-off a comparison is made between all the possible ventilation solutions based on nine different criteria(Appendix 12: Heating & Ventilation Trade-off). The result of this trade-off is shown in the figure below (*Figure 43*). The working of a trade-off, is described in chapter 5.2.2 Heating trade-off. The ventilation trade-off contains one more criteria than the heating trade-off, namely the humidity control.

Constantialization		Natural			2
Spot ventilation	Mechanical	Solar-air heat		130	1
Multiple room ventilation	Natural	Bala	nced HRV	106	5
		Delegend	HRV	114	3
	Markenterl	Balanced	ERV	108	4
	iviecnanical	Only	Only air supply		6
		Only e	exhaust air	100	6

Figure 43: Ventilation trade-off

The first main distinction that can be made by the possibilities is the amount of rooms that need to be ventilated. Single room called 'Spot ventilation' and multiple room ventilation. These distinctions can both be divided into natural and mechanical ventilation (see chapter 4.3.1 Natural vs. Mechanical Ventilation).

Solar-air heat

The trade-off contains a spot ventilation solution called solar air heat. It is a system in the form of a rectangular panel that uses solar radiation to heat up air and blows it into the building.

Solarventi Ltd. is a company in Denmark that has invented and sells these solar-air heat panels. A Solarventi panel is an 'efficient air-based solar collector, which would operate solely on sunlight and independently of connection to the mains supply.' (Solarventi, n.d.). A solarventi panel (Figure 44) consists of three parts.

- Hot air collector
- Small solar panel
- Fan



Figure 44: Solarventi Panel (Solarventi, n.d.)

Air is let in through the backside of the panel by a special perforated aluminum plate. The Sun heats a black felt mat. The warmth of this black felt math is transferred to the air that is sucked in. The warm air is blown into the building by a fan. The fan is powered by a small solar panel that is integrated on the front side of the panel. The airflow is between 25 and 150 cubic meter with a temperature rise between 15 and 40 degrees Celsius. The amount of airflow can be changed, the smaller the airflow, the higher the temperature of the air that is forced in.

Based on the results of the trade-off, the Solarventi panels (*Figure 45*) are the best solution. However, these panels are made to prevent moist in single spaces and small buildings, such as summerhouses, garages, caravans and even boats. Since the buildings on the islands are substantially bigger and they contain a lot of different rooms, this solution will not be used as the main ventilation system.

Later in the report (in chapter 5.3.3 Rain penetration/ specific solution) this system is chosen to prevent rain from penetrating into the southern walls and to force the moist in the walls back out.



Figure 45: Solarventi (Svångemåla News, 2010)

Conclusion

The first discarded solutions are (see red cells in Figure 43):

- Natural spot ventilation
- Multiple room Natural HRV
- Air supply ventilation

Natural spot ventilation is discarded due to the high heat losses and no possibility to control the air inlet and outlet. **Multiple room natural HRV** is a system that is driven by internal building airflows. These flows are induced by the wind blowing onto the building (pressure difference) and the density difference between warm and cold air. If the airflows in the building are not sufficient, fans are used as flow controllers. This system is not likely to be used in existing buildings, as it requires a close integration with the building design (Eimund Skåret, Peter Blom, Trygve Hestad, n.d.).

For this reason, and because of the total absence of data about the airflows inside the buildings in the archipelago, this solution is discarded. Air supply ventilation is not likely to be used in cold climates because the system has the potential to cause moisture problems in cold climates. It also requires maintenance of the filter system for the incoming air, and it contributes to higher heating costs because of the absence of a heat recovery system.

Among the remaining solutions the best solution is the balanced HRV. This system is equipped with a heat exchanger that transfers the heat of the outgoing air to the incoming air. This results in a substantial decrease of the heat losses and heating costs.

5.3.3 Rain penetration

Rain Penetration refers to 'ingress of rainwater above ground at various points in the external envelope of the construction that is through roofs, walls, chimneys and openings such as windows and doors'. (The Society for the Protection of Ancient Buildings, n.d.)

Rain penetration is caused by three main factors: water on the outside walls, openings and permits to passage and forces that drive the water in the walls. If one of those three factors is removed, the rain penetration problem is eliminated.

Water on the outside walls

Driving Rain is typically the largest source of moisture for the above-grade building enclosure. The control of management of rainwater should be one of the most important considerations for designers. (Ontario Association of Architects, n.d.) In this report the design of the buildings is not taken into consideration; the buildings in this project are already built. The buildings in the archipelago are left to their autonomous systems of preservation during the winter. The elements cannot be stopped, but there are measures that can be taken to prevent water being on the walls after the building stage. These solutions will be presented later in this report.

Openings to permit Passage

Openings that permit the passage of water are quite numerous on the face of a building in the form of pores, cracks, poorly bonded interfaces and joints between elements or materials. (G.K. Garden, 1963) Smalls cracks and joints can be covered with impermeable or semi-impermeable coatings. This is difficult to achieve, as the coatings have to be applied perfectly. Maintenance of a perfect joint is even harder due to differential movements between parts and different flex levels of the materials.

Covering the complete building with an impermeable sealant is not a solution. Old buildings need to 'breathe'. The moist that is forced in has to evaporate back out.

Forces that drive the water in the walls

Rain Penetration will only occur when there is a force available to move the water through the opening. This force can be gravity, kinetic energy of the raindrops, capillary suction and air pressure differences. Air pressure differences are produced by wind blowing at the walls. Relatively low velocity airflow can also carry fine water droplets or snow into the wall to create the same problem. Water can be raised a considerable distance and caused to flow into a wall when an air pressure difference is added to capillary suction. (G.K. Garden, 1963)

General Solutions

General solutions applied to the problem of rain penetration can be classified in three main solutions:

- Deflection
- Drainage
- Drying

Deflection can be realized by multiple solutions. Landscaping and chosen site are of great importance of deflecting the wind over or along the building. Next step of deflection is the design of the building. Overhanging roofs protect the wall from direct winds. As seen in *Figure 46* the size of the overhang correlates directly with the probability of rain-related damage. (Ontario Association of Architects, n.d.)



Figure 46: Roof overhang (Ontario Association of Architects, 2012)

Drainage assumes that the water will penetrate the outer surface but will be removed by an assembly within the wall. Wood and masonry leak significant amounts of water



Figure 47: Screen drained walls (Ontario Association of Architects, 2012)

The design of screen-drained walls is most realistic and practical. In this case this would be useless, as the building exists already. *Figure 47* shows different options of screen drained walls.

Despite all efforts to deflect and drain the rainwater, field experience has shown that some water always penetrates into the walls. A **Drying** solution has to be provided for this water. Moisture can be removed out of walls by:

- 1. Evaporation
- 2. Vapor transport
- 3. Drainage
- 4. Ventilation



Figure 48: Drying mechanism in walls (Ontario Association of Architects, 2012)

Figure 48 shows that **evaporation** can occur from the inside or outside surfaces. **Vapor transport** can occur by diffusion, air leakage or both. **Drainage** is the fastest method of removing large amounts of water. Thereby it is one of the most important measures against rain penetration. Removing all water is impossible due to the capillary forces and the absorbance of the materials. **Ventilation** in the form of air movement or diffuse drying can only remove the remaining water. Air movement can move a large quantity of water. It is however hard to control the airflow, expensive in terms of energy and potentially dangerous for the quality of the air inside. (Ontario Association of Architects, n.d.) A modern approach is therefore to limit the airflow through the walls to nearly zero. Diffuse drying can transport moisture in both ways through the wall. In cold weather the moisture is forced outside, and in warm weather the moist is forced inside the building. Inward drying is an important mechanism for sustaining buildings.

Weather Archipelago



The Kvarken archipelago has an annual precipitation of 500 / 550 mm (Figure 49).

Figure 49: Precipitation data (World Weather and Climate Information, 2009)

As seen in the figure, most of this precipitation falls during the summer months.

The building is heated to five degree Celsius for maintenance purposes. During the months when it is colder, the wind is 6,5 m/s on average with mostly southern directions (*Table 19*).

Month	AVG [©] C	AVG wind direction	AVG wind speed (m/s)	Probability wind speed >8 m/s(%)
November	+2	ENE	7,2	49
December	-2	SSE	7,2	66
January	-3	SE	6,7	50
February	-7	S	6,1	39
March	-1	WSW	6,7	48
April	+2	SSW	5	32

Table 19: Wind direction and speed

Table source: (WindFinder, 2012)

This means that the southern walls are mostly exposed to the rain/snow and wind during the winter season.

The south walls are not only exposed to the wind and precipitation, but also to the sun. This can be used as an advantage of the building. The shortest amount of daylight during winter in the archipelago is 4.11 hours (*Figure 50*).



Figure 50: Daily hours of sunshine and twilight (WeatherSpark, 2012)

This sun can be changed into energy by the use of solar panels.

Specific Solution

The data above shows that the southern walls are mostly exposed by precipitation and wind. An advantage of this climate is that these walls are exposed to the sun as well. Deflection by landscaping is hard in the archipelago. The vegetation has a hard time growing due to the cold climate and the rocky ground. A fence to deflect the wind will work, but will pollute the view of the archipelago. Drainage of rainwater is taken care of in the design stage of the building. The roofs do have an overhang and drainage can occur by gravity. Therefore to get rid of the problem of rain penetration, the ventilation should be improved.

The use of **Solarventi** panels can protect the southern walls from rain penetration and provide extra heat and ventilation to dry the walls and eliminate the moist (more information about these Solarventi panels can be found in chapter 5.3.2, Ventilation trade-off / Solar-air heat). The panels are maintenance free and work autonomous. In the archipelago this is a great advantage, as it is impossible to go to any of the islands, due to the ice conditions during the winter. Even when the complete power and heating systems shuts down, a little heating and ventilation will occur by using these panels.

5.4 Control and monitoring system

The location of the islands makes it difficult to reach the installations during the winter months. Due to this fact the systems needed to be automated and remotely controllable. Since the solutions consists of several different subsystems, a monitoring system was necessary to control the power distribution as well as the heating and ventilation systems.

The table below shows the active elements of the system.(Table 20)

Table 20: Active elements of the system

Main power system	Secondary power system	Heating and Ventilation
Wind Turbing	Electrolyzer	Heat Pump
Selar Panels	Hydrogen Tank	Water Accumulator
	Fuel Cell	Radiators Pump
	*Emergency Generator	Ventilation Fans

The basics of the automated functioning of the system goes as follows:

- There is a main switch to turn the whole power system ON or OFF.
- There is an individual switch to turn each sub-system ON or OFF.
- When the Production (Wind Power and Sun Power together) are bigger than the building Demand, the extra electricity goes to the Electrolyzer, and therefore Hydrogen is produced.
- This will stop when the Hydrogen Tank is full (objective pressure is reached, 30 BAR), or when the Production (Wind + Sun) is again smaller than the Demand.
- When the Production is smaller than the Demand, the Fuel Cell will start taking Hydrogen from the Hydrogen Tank and with that, produce electricity. This will go until the Demand is smaller than the Production again.
- The Emergency Generator will start producing electricity if the Hydrogen tank empties (pressure drops below minimum for the Fuel Cell), or if the Fuel Cell is OFF.
- The Heat Pump will start heating up water when the temperature in the Water Accumulator drops below the minimum set (40°C) and stop when it rises above the maximum set (50°C).
- The Radiator's pump will make the water from the accumulator run when the Inside Temperature drops below the minimum set (5°C) and stop when it rises above the maximum set (10°C).
- The ventilation system will run for 1 hour twice a day or when the humidity reaches a determined level (to be determined) and stop when it goes below the minimum acceptable level (to be determined).
- There will be a Safety system monitoring the operating temperatures of the elements in the system, which will shut the element down and send a warning signal to the monitoring station.
- There will be a Safety system monitoring the concentration of Hydrogen, so if it reaches a level above the acceptable, the Hydrogen sub-system will be shut down and a warning signal will be sent to the monitoring station.

- There will be a Safety valve in the Hydrogen Tank that will release hydrogen, if for some reason the pressure in the tank goes above the limit set for the input from the electrolyzer (30 BAR for the electrolyzer output, 35 bars for the security valve).
- There will be a manual Stop command, which will stop all the sub-systems until a manual Start is done again. (System ON/OFF switch).

To do that, several sensors of different types will be needed. These are the minimum amount of sensors needed for an automated operation. If any other parameters are needed or wanted. The sensor net can easily be upgraded.

Below there is the list of sensors necessary, with the denomination used in the Grafcet (Table 21).

TEMPERATURE SENSORS	FLOW-METER
T _{in}	Eproduction
T _{out} T _{0m} T _{60m} T _{120m} T _{accumulator}	LEVEL-METERS
	Accumulator level Pure water tank level Emergency generator fuel level
	HYGROMETER
T _{H2tank}	
l fuel cell T _{water tank}	Н
PRESSURE SENSOR	H ₂ CONCENTRATION METER
P _{H2T}	H _{2 concentration}

Table 21: List of sensors organized by type

With those sensors there will be enough data to monitor. These sensors are not only used mainly for operating or safety reasons, but also to have a data log of the parameters of the system (live data, averages, peaks...)

The following table shows the proposed monitoring parameters.

Table 22: Monitoring Layout Example

POWER SYSTEM	ON/OFF				
WIND TURBINE	ON/OFF		Enabled/Disabled		
SOLAR PANELS	ON/OFF		Enabled/Disabled		
ELECTROLYZER	ON/OFF		Enabled/Disabled		
FUEL CELL	ON/OFF		Enabled/Disabled		
HEAT PUMP	ON/OFF		Enabled/Disabled		
RADIATORS PUMP	ON/OFF		Enabled/Disabled		
VENTILATION	ON/OFF		Enabled/Disabled		
			WIND TURBINE POWER week average	#	W
			WIND TURBINE POWER month average	#	W
WIND TRUBINE POWER	#	W	WIND TURBINE ENERGY 24h	#	Wh
		Enabled/Disabled Enabled/Disabled Enabled/Disabled Enabled/Disabled Enabled/Disabled Enabled/Disabled Enabled/Disabled WIND TURBINE POWER week average # WIND TURBINE ENERGY 2Ah # WIND TURBINE ENERGY Chall # SOLAR PANELS POWER week average # SOLAR PANELS POWER month average # W SOLAR PANELS ENERGY total # Wh SOLAR PANELS ENERGY total # Wh POWER DEMAND month # Wh ENERGY DEMAND month # Wh ELCTROLYZER PRODUCTION week average # W FUEL CELL PRODUCTION month average # W FUEL CELL PRODUCTION month average			
			WIND TURBINE ENERGY total	#	Wh
			SOLAR PANELS POWER week average	#	W
			SOLAR PANELS POWER month average	#	W
SOLAR PANELS POWER	#	w	SOLAR PANELS FORERGY 24h	#	Wh
		••	SOLAR PANELS ENERGY month	#	Wh
			SOLAR PANELS ENERGY total	#	Wh
					14/
			POWER DEMAND week average	#	VV VV
POWER DEMAND	#	W	FOUR DEMAND month average	#	VV VV
			ENERGY DEMAND month	#	Wh
			ENERGY DEMAND LOCAL	#	VVII
			ELECTROLYZER PRODUCTION week average	#	l/min
ELECTROLYZER PRODUCTION	#	l/min	ELECTROLYZER PRODUCTION month average	#	l/min
			ELECTROLYZER PRODUCTION total	#	I
ELECTROLYZER TEMPERATURE	#	°C			
			FUEL CELL PRODUCTION week average	#	W
FUEL CELL PRODUCTION	#	W FUEL CELL PRODUCTION month average	FUEL CELL PRODUCTION month average	#	W
			FUEL CELL PRODUCTION total	#	Wh
FUEL CELL TEMPERATURE	#	°C		#	
H2 STORAGE	#	Kg			
H2 STORAGE PRESSURE	#	BAR			
H2 STORAGE TEMPERATURE	#	⁰C			
H2 CONCENTRATION IN AIR	#	%			
			TEMPERATURE INSIDE week average	#	°C
TEMPERATURE INSIDE	#	°C	TEMPERATURE INSIDE month average	#	°C
				#	90
TEMPERATURE OUTSIDE	#	°C		#	<u>-</u> €
				#	-0
HUMIDITY IN WALLS	#	%	HUMIDITY IN WALLS week average	#	%
			HUMIDITY IN WALLS month average	#	%
	#	٥C	TEMPERATURE GROUND week average	#	°C
	π	-0	TEMPERATURE GROUND month average	#	°C
			TEMPERATURE 50m week average	#	°C
TEMPERATURE 60m	#	ēC	TEMPERATURE 50m month average	#	°C
			TEMPERATURE 100m week average	#	٩C
TEMPERATURE 120m	#	°C	TEMPERATURE 100m month average	#	°C
					÷
	#	I			
TEMP	#	°C			
	#	1			
PURE WATER TANK TEMP.	#	≌C			

Most of the elements composing the system will be able to be over-ridden remotely, either by turning them ON or OFF, if this is considered necessary for any reason.

The over-ride feature will be for these elements:

- SYSTEM
- WIND TURBINE
- •SOLAR PANELS
- ELECTROLYZER
- FUEL CELL
- •HEAT PUMP
- RADIATORS PUMP
- VENTILATION

The sensors and switches placing can be seen in the SENSOR DIAGRAM (Appendix 13). The basic layout for the CONTROL SYSTEM will as seen below, divided by independent sub-systems. It is written as GRAFCETs, so it can be implemented in any PLC later (*Figure 51 - 57*).

Power distribution

WAIT		
START		
	1	
(W + S) > 0		
(W+S < D) AND (HT > 30 bar) OR (Eoff) (W+S < D) AND (HT > 5 bar) (HT < 5 bar) OR (FCoff))		
WAIT FUEL CELL EMERGENCY GENERATOR		
HT < 25 bar (W+S > D) OR (FCon)	STOP	LEAK > ?
		LEAK WARNING
		STOP

Figure 51: Power Distribution Grafcet

Heat pump operation



Figure 52: Heat Pump Operation Grafcet

Radiators Pump Operation





Ventilation Opearation



Figure 54: Ventilation Operation Grafcet

6 Results

The result of this project is a solution for the energy needs for the buildings in the islands, both for heating and for electricity. It accomplishes the initial goals, being a sustainable, autonomous, remotely controllable and reliable system. There a two generic solutions for different energy needs ranges and two specific solutions for Mickelsörarna and for Valsörarna.

In this chapter every solution is described in detail. An overview of the differences between the different solutions can be seen in Chapter 6.5, Summary.

6.1 Final concepts

6.1.1 Generic solution small

Electricity

Primary system

This is a generic solution for a system with less than 6kW of energy needs. The electrical system should supply around 3,5 kW. The range for the wind turbines is not detailed. The difference between the sizes of the wind turbines is big. It means that the wind turbine could oversupply the installation. However, when a smaller device is not enough, it will be necessary.

This generic solution contains a hybrid system composed of a wind turbine with a power output of 10 kW and solar panels with a power output of 6 kW. The turbine's manufacturer is Anhui Hummer Dynamo Co. LTD, the model is H8.0 10kW. The complete wind turbine's datasheet is found in *Appendix 14: Wind Turbine Datasheet*. The solar panels' manufacturer is Xuzhou Aibo Energy Technology Co. LTD, the model is AB200M and the provider of these solar panels is a company from Vasa called Sunergy, A.Y. A datasheet of solar panels is shown in *Appendix 15: Solar Panel Datasheet*.

The amount of energy obtained from this system depends on the period of the year. During winter the Power output is around 4.8 kW and during the summer the Power output is around 3.5 kW. This means that the energy obtained is considerable higher during the winter.

The price of the wind turbine depends on the type of installation. The total price with a single-phase converter is **12634,45** and the price with a three phase converter is **13178,98**. Transportation costs from Shanghai to Helsinki is **196,09**. The detailed budget of the wind turbine and transportation is shown in *Chapter 6.1.3 Mickelsörarna*.

The price of the solar panels is approximate. The exact price is obtained when the panels are ordered. One system of 6 kW solar panels and 2 pieces Outback 80 Flexmax regulators cost around 10.000 €, transportation to Vasa included.

Secondary system

For a smaller generic solution, the brief data of each component is listed in the following tables. More detailed data sheets will be found in Appendix 17: Electrolyzer Datasheet.

Table 23: Electrolyzer-Acta AES200

Company	Acta Energy
model	AES200
H2 production rate	200 l/h
Standard working pressure	15 bar
Maximum allowable pressure	30 bar
purity@30 bar	99.94 %
Purity with additional purification	99.999 %
Water consumption	0.16 l/h
Water conductivity@20 °C	5-10 µS/cm (Distilled water only)
Power consumption	1060 W
Dimension-(AxBxC)	180mm x190 mm x300 mm
Weight(without water)	20.5 kg

Table source: (Acta Energy, n.d.)

Table 24: Hydrogen tank for smaller generic solution

Volume	< 15000 liters
Pressure	30 bar
Stored temperature	ambient temperature

As regards the fuel cell, the company is called ReliOn. ReliOn focuses mainly on the telecom and military markets. They make fine products for stationary applications as well. Their fuel cells have high quality and different outputs. They allow the customer to configure the product to suit the load. For the smaller generic solution, where the electricity needs is smaller than 3.5 kW, ReliOn T-2000[®] 4kW Outdoor Configuration is chosen. Two ReliOn T-2000(2 kW) fuel cells consist of one ReliOn T-2000[®] 4kW Outdoor Configuration. The data is listed below in *Table 25*.

Table 25: Fuel cell-ReliOn T2000®4kW outdoor configuration

Company		ReliOn			
Model		ReliOn T-2000	ReliOn T-2000 [®] 4kW Outdoor Configuration		
Physical	Dimensions (w x d x h)	53.3cm x54.6cm x 66cm	183cm x137cm x 104cm		
	Weight	61 to 110 kg			
	Mounting	23" rack mount			
Dorformonco	Rated net power	0 to 2 kW	0 to 4 kW		
Performance	Rated current	0 to 40A@48VDC			
	DC voltage	24 or 48 VDC nominal	24 or 48 VDC nominal		
	Composition	Purity 99.95%	Purity 99.95%		
Fuel(H ₂)	Supply pressure to unit	0.24 to 0.41 bar	0.24 to 0.41 bar		
	Consumption	30 slpm @ 2 kW	30 slpm @ 2 kW		
	Hydrogen storage capacity	n/a	n/a		
	Ambient temperature	2°cto 46°C	-40°Cto 46°C		
Operation	Relative humidity	0-95% non-condensing			
	Altitude	-60m to 4206m			
	Location	Indoors	Outdoors		
Safety	Compliance	UL/CSA/CE	NEBS Level3/Seismic Zone 4		
Emissions	Water	Max.30mL/kWh			
Emissions	Noise	53 dBA @3.28 ft/1			
Monitoring	Remote	System configuration& status/historical& operational data	Capability		
	Communications	KJ45/DB9/Dry Contact			

Table source: (ReliOn, Inc, 2012)

Heating & Ventilation

For the **heating** of the generic solution, the assumption has been made that the building contains an existing radiator system. The hot water that is needed in this system will be provided by a GSHP in connection with an accumulator. The accumulator contains a water/glycol mixture to prevent the fluid of freezing. To obtain a minimum inside temperature of 5 °C, the mixture will be heated to 45°C.

A Finnish company named Gebwell Ltd will provide the used HP installation. The company is specialized in environmentally friendly solutions for heating and cooling (Gebwell.Ltd, n.d.).

The specific HP type is the Gebwell T6. This HP has a heat output of 6kW and a COP of around 3. The volume of the accumulator is 1000 liters. More technical information about the HP is found in Appendix 12, Heating and Ventilation Trade-off.

For the **ventilation** of the generic solution the assumption has been made that the building had no existing ventilation system. The chosen system is an HRV system. The manufacturer of the ventilation components is FläktWoods. They provide a wide range of ventilation and heat recovery equipment. Retailers can be found in Turku and Espoo, Finland (Flaktwoods, n.d.).

The solution is presented below. Figure 55.



Figure 55: Generic heating and ventilation solution

A summary of the used heating and ventilation equipment for the small generic solution is shown below *Table 26*.

Generic solution small					
	Total area			/	
Building	Total volume			/	
		Heating demand		>6kW	
			Heat source	Ground	
			Propreties	Vertical	
				Closed loop	
			Manufacterer	Gebwell Ltd.	
	Heat	pump	Туре	Gebwell T6	
			Heating output	6kW	
			СОР	3	
Heating			Power	2kW	
-			Borehole depth	120m	
			Pipe length	/ / / SekW Ground Vertical Closed loop Gebwell Ltd. Gebwell Ltd. Gebwell T6 6kW 3 2kW 120m Gebwell Gebwell Mater-glycol 6 Water-glycol 6 Fuel cell 45°C/30°C Opening the windows Cracks in the walls / / / / / //	
			Manufacterer	Gebwell	
	Heat storage	Accumulator	Accumulator Volume 100	1000	
	-		Contents Water-glycol		
		Back-up resistor		6	
	Exhaust heat re		Heat source	Fuel cell	
	Heat output		Radiators	45°C/30°C	
		Na	atural	Opening the windows	
				Cracks in the walls	
	Air supply		Ducts	/	
		Mechanical	Fans	/	
			Pipes	/	
Ventilation			Ducts	/	
			Fans	/	
	Exhaust air	Mechanical	Pipes	/	
			Moist control	/	
			Clock system	2h/day	
	Heat r	ecovery	Туре	Rotary heat exchanger	
			Manufacterer	Fläktwoods	

Table 26: Heating and ventilation for generic solution small

6.1.2 Generic solution big

Electricity

Primary system

This generic solution has been calculated for an installation from 6 to 10 kW. The electrical installation should cover an energy need from 3.5 to 5 kW. This solution is calculated in a way that supplies around 5 kW of energy all year round. The electrical needs are similar to those on Mickelsörarna. The components of the primary energy system are the same; a hybrid system composed of a 10 kW wind turbine and a 12 kW solar panel.

The wind turbine is the model H8.0 10kW from Anhui Hummer Dynamo Co. LTD. The complete datasheet is found in *Appendix 14, Wind Turbine Datasheet*. The solar panel is model AB200M from Xuzhon Aibo Energy Technology Co. LTD, the provider is a local company from Vasa called Sunergy, A.Y. The complete datasheet is found in *Appendix 15, Solar Panel Datasheet*. Both devices are made in China. In *Chapter 6.1.3, Mickelsörarna* there are tables and graphs about the energy produced by these devices.

The price of the wind turbine depends on the type of installation. The total price with a single-phase converter is **12634,45**. The price with a three phase converter is **13178,98**. Transportation costs from Shanghai to Helsinki are **196,09**. A detailed budget of the wind turbine and transportation is found in *Chapter 6.1.3, Mickelsörarna.*

The price of solar panels depends on multiple factors. The exact costs can only be given when the panels are ordered. The approximate price for a 12 kW solar panel with 3 Outback 80 Flexmax regulators is about **20.000€**. Transportation to Vasa is included in the price.

Secondary system

For the bigger generic solution, the same electrolyzer is chosen as shown in *Table 23*. The following tables show the rest of the components.

Table 27: Hydrogen tank for bigger generic solution

Volume	15000 liters – 20000 liters
Pressure	30 bar
Stored temperature	ambient temperature

A fuel cell called DBX5000 from a company named Dantherm is chosen. The following table lists its main parameters.

Company	Dantherm			
model	DBX5000			
Power output	W	Continuous	5000	
Voltage output	VDC	Fixed within	-47 to -57	
Voltage input	VAC	For standby operation	90 – 264/50-60Hz	
Hydrogen purity	%	Commercial grade 3.5	Min 99.95	
Inlet pressure	Barg	Nominal to valve block	5	
consumption	Nm³/kWh	Average at max. load	0.95	
Ambient temperature	°C	Operational(optional)	-20(-40) to +40(-55)	
Integration cabinet	°C	Operational	0 to +60	
Storago tomporaturo	ଂମ	Weather protected	45 130	
Storage temperature	L			
Cabinet dimensions	mm	H x W x D 611 x 500(450) x 555		
Weight	Kg	Stand alone module	75 kg	
Ingress protection	IP-class	External to internal	55	
Air flow	m3/h	Exhaust to outside	200-1600	
Backup start up time	Sec.	Depends on batteries	Installation dependent	
Interface/system		Standard configuration RJ45 TCP/IP –CAN Bus		
monitoring	-	Display panel		
Voltage free outputs alarms	-	Goes open on fault DB15 with 4 channels		
Visual indication alarms	-	display	1	
Interface- DC	-	On front panel 175 Amp Anderson type		
Interface- AC(only DIB version)	-	On front panel	IEC 320 C14	
Hydrogen	Fitting	-	8 mm Tube	
	DBX requires fresh air supply and ducting of exhaust air to outside ambient.DBX can only work when equipped with Dantherm Power Valve Block and a fuel regulator supplied by or approved by Dantherm Power			
Important note				

Table source: (Dantherm Power A/S, 2009)

Heating & Ventilation

For the big generic solution an HP with 10kW heat output is used, namely the Gebwell T10. Technical information about the HP is found in *Appendix 12, Heating & Ventilation Trade-off*.

The **ventilation** system is identical to the one used the small generic solution (see chapter 6.1.1, Generic solution small/ Heating& Ventilation). The presentation of the heating and ventilation system is the same as in *Figure 54*. A summary of the used heating and ventilation equipment for the small generic solution is shown in the following table (*Table 29*).

Generic solution big				
Building	Total area and volume			/
	Heating demand		6-10kW	
			Heat source	Ground
			Propreties	Vertical
				Closed loop
			Manufacterer	Gebwell Ltd.
	Heat p	ump	Туре	Gebwell T10
			Heating output	10kW
			СОР	3
Heating			Power	3,3kW
5			Borehole depth	120m
			Pipe length	240m
		Accumulator	Manufacterer	Gebwell
	Heat storage		Volume	20001
			Contents	Water-glycol
			Back-up resistor	6
	Exhaust heat recovery		Heat source	Fuel cell
	Heat ou	itput	Radiators	45°C/30°C
		Natural		Opening the windows
				Cracks in the walls
	Air supply Mec		Ducts	/
		Mechanical	Fans	/
			Pipes	/
Ventilation			Ducts	/
			Fans	/
	Exhaust air	Mechanical	Pipes	/
			Moist control	/
			Clock system	2h/day
	Heat recovery		Туре	Rotary heat exchanger
			Manufacterer	Fläktwoods

Table 29: Heating and ventilation solution for generic solution big

6.1.3 Mickelsörarna

Electricity

Primary system

Mickelsörarna is currently powered by a hybrid method. There are two diesel generators, a 75kW generator and a 50 kW generator. To reduce the use of the generators a model of the Whisper 500, 3.2 kW wind turbine and 21, 100 Watt PV solar panels is installed. As back up a fluid Solar 1500 battery bank has been installed. The battery has a maximum discharge of 70%. Therefore the control unit is programmed to start the generator when the battery is discharged to 35% (Tuomo Riikonen, 2008)

The generators are old and oversized. The efficiency is therefore, less than 30%. The fuel consumption on Mickelsörarna was 76.250 liters between 1997 and 2007. The generators consume about 6 liters per hour. The high consumption of fuel and the price of transportation results in high costs for the owner.

Another significant cost is the maintenance of the generator. The costs of maintenance between 1997 and 2007 were 17.400. The maintenance of the generators accounts 80% of the total maintenance costs. Furthermore, the old diesel generators have a high level of pollution.

The primary system that will be used is hybrid. For this project hybrid means, composed of a Wind Turbine and Solar Panels. The wind turbine produces more energy in winter, in contrast to the solar panels that only create significant energy in summer. By using a hybrid system, the different energy needs for summer and winter will be covered.

• Wind Power

The turbine chosen is *H8.0 10000W* from the company *Anhui Hummer Dynamo Co. LTD.* The turbine has been selected for the reason that the power curve is very suitable for the wind speed averages on Mickelsörarna. Furthermore, this device has a good efficiency and a small size, the tower is 12 meters high. The complete datasheet of the turbine is found in *Appendix 14, Wind Turbine Datasheet*.

The total amount of energy obtained is higher in winter than in summer. In winter there is, on an average, more wind. The wind turbine produces more energy in winter then it does in summer. The energy needs have seasonal differences, hence the reason to go hybrid. During the winter the wind turbine is the main source of energy, it should therefore supply most of the energy demand. During the coldest weeks however, there are periods without wind. During the winter the energy required is approximately 100 kWh/day. The energy obtained from the wind turbine is calculated as follows:

Firstly, the Power Out of the turbine is calculated for each month, based on the Power curve of the Wind Turbine and the wind speed average [1]. Then, the amount of energy obtained by the wind turbine is calculated per month:

Wind Energy per Month = Power Out x 24 hours x Days [1]

The Power-Out of the turbine is multiplied by the number of hours in a day and the number of days in that specific month. The sum of these calculations (*Table 30*) gives the total amount of energy that can be obtained from the wind using a Wind Turbine per year. (*kW/h*)

Month	Wind Speed (m/s)	Power Out (W) [1]	Energy Wind (kWh/month) [2]
January	6,8	3900	2808
February	6,2	3400	2448
March	5,7	2900	2088
April	5,3	2200	1584
May	4,9	1800	1296
June	4,7	1600	1152
July	4,6	1450	1044
August	5,1	2000	1440
September	5,9	3000	2160
October	7	4200	3024
November	7,4	4600	3312
December	7,2	4400	3168

Table 30: Wind energy per month summary

The following figure shows the curve of wind energy during the year. It shows the difference between winter and summer months regarding the obtained energy.



Figure 56: Wind energy per year curve

The total price of the wind turbine depends on the type of installation. There is a total price for single-phase installation and a different price for three-phase installation. Both budgets are shown in the next table (*Table 31*).

Table 31: Wind turbine H8.0 budget

WIND TURBINE: H8.0 10000W				
Wind turbine	8.038,00 USD	6062,30€		
PLC Controller	836,00 USD	630,52€		
Gried Tied Rectifier	630,00 USD	475,15€		
Dumping Load	801,00 USD	604,12€		
Gried Tied Converter (singe phase)	4820,00 USD	3635,27€		
Gried Tied Converter (three phase)	5542,00 USD	4179,80€		
12m guyed tower	1627,00 USD	1227,09€		
TOTAL (single phase converter)	16752,00 USD	12634,45 €		
TOTAL (three phase converter)	17474,00 USD	13178,98 €		

This price is free on board Shanghai. The transportation from Shanghai to Helsinki costs 65 USD/CBM. The total volume of the turbine is 4 CBM, meaning that the transportation will cost 260USD, (**169,09€**). This shipping price does not include any port costs in Helsinki, e.g. customs cost, import duties, etc.

• Solar Power

The Solar Panel chosen comes from a company called *Xuzhou Aibo Energy Technology Co.,Ltd.* located in China. The model of the device is *AB200M*. The budget, advice and datasheet were obtained from a local company in Vasa specialized in Solar Panels. The company is called *Sunergy a.y.* The complete datasheet of the solar panels is found in *Appendix 15, Solar Panel Datasheet*.

The main reasons for choosing these solar panels are: warranty of order, good quality of performance, and good cell efficiency: 17.9%. The cell efficiency is an important factor. It is a calculation on the capacity of the exploitation of the received insolation. This system has 60 units of 200W solar panels, multiplying this numbers calculates that this solar system has 12.000W of power.

Solar panels are only usable during the spring and summer months. In that time of the year the insolation is sufficient to obtain a significant quantity of energy. With the data of the solar insolation the amount of energy that the solar panels can obtain from the sun is calculated with equation [2]

Total Energy obtained = Insolation x Total Area x Efficiency [2]

The insolation data is per square meters, and it is necessary to know the total area of the solar panels. The area that this system covers is calculated with equation [3] by using the data on the datasheet of the solar panels:

Total Area = 60 solar panels
$$x \frac{1.27664m^2}{solar panel} = 76.5984 m^2$$
 [3]

The total insolation that the solar panels receive is calculated by knowing the total area of the system and the monthly insolation data (*Appendix 07: Weather Data*). The following step is to take the efficiency of the solar panel into account (*Table 32*).

Table 32: Salar energy per month

Month	Insolation (kWh/m²)	TOTAL SIZE SOLAR PANELS* (m ²) [1]	EFFICIENCY (%)	SOLAR ENERGY (kWh) [2]
January	4,03	76,5984	17,9	55,25578781
February	19,6	76,5984	17,9	268,7378266
March	56,11	76,5984	17,9	769,3305841
April	110,7	76,5984	17,9	1517,820276
May	163,68	76,5984	17,9	2244,235074
June	177,3	76,5984	17,9	2430,980441
July	168,33	76,5984	17,9	2307,991752
August	124,93	76,5984	17,9	1712,929422
September	72,6	76,5984	17,9	995,4268474
October	30,69	76,5984	17,9	420,7940764
November	8,7	76,5984	17,9	119,2866883
December	1,55	76,5984	17,9	21,25222608

The following figure shows the amount of energy obtained from solar panels all year round.



Figure 57: Solar energy per month curve

The exact price of the solar system can be given when the order is placed. This is because prices change frequently. They depend on e.g. the stock at the storage and other variable factors.

The total price of the solar system containing 12 kW Solar Panel and 3 pieces Outback 80Flexmax regulators will be around **20.000€**. The transportation to Vasa is included in this price.

Secondary system

Electrolyzer for Mickelsörarna can be seen in Table 23. The fuel cell is also the same for the big generic solution, which can be seen in *Table 28*. The following table shows the hydrogen tank *(Table 33)*.

Table 33: Hydrogen tank for Mickelsörarna

Volume	~20000 liters
Pressure	30 bar
Stored temperature	ambient temperature

Heating & Ventilation

The **heating** solution for Mickelsörarna is a Gebwell T10 HP connected to a 2000-liter water accumulator. The accumulator is already present in the building from the previous heating system. It is equipped with a back-up resistor and connected to an exhaust heat recovery system that provides extra heat from the fuel cell. The accumulated hot water will be used in the existing radiator system.

The **ventilation** system is already installed in the building. It is an exhaust ventilation system with tubes that only go to the kitchen, bathrooms and storage rooms. Fresh air comes into the building through cracks, small holes, and openings around doors or by opening a window. The building requires one total air renewal every day. Therefore, the fans will work two hours a day. The system will be equipped with a humidity control system that turns the fans on whenever the humidity inside the building reaches a set level.

The following figure shows the heating and ventilation solution for Mickelsörarna (Figure 58).



Figure 58: Heating and ventilation solution for Mickelsörarna

A summary of the used heating and ventilation equipment for Mickelsörarna is shown in *Table 34* below.

Mickelsörarna				
	Total area			689 m²
Building		Total volume		
	H	leating demand		6 kW
			Heat source	Ground
			Propreties	Vertical
				Closed loop
			Manufacterer	Gebwell Ltd.
	Heat pur	ιp	Туре	Gebwell T10
			Heating output	10kW
			СОР	3
Heating			Power	3,3kW
			Borehole depth	120m
			Pipe length	240m
	Heat storage Accumulator		Volume	2000
		Accumulator	Contents	Water-glycol
			Back-up resistor	6
	Exhaust heat recovery		Heat source	Fuel cell
	Heat output		Radiators	45°C/30°C
	Air supply		Natural	Opening the windows
				Cracks in the walls
				Storage rooms
			Ducts	Bathrooms
Ventilation				Kitchen
	Exhaust air	Mechanical	Fans	
			Pipes	
			Moist control	
			Clock system	2h/day
	Heat recovery			/

Table 34: Data o	f heatina	and ventilation	solution f	for Mickelsörarna
Tubic 34. Dulu 0	j neuting	and ventilation	solutionj	or where is or arma

6.1.4 Valsörarna

Electricity

Primary system

The electrical needs for Valsörarna are calculated with the evaluation model. There is a big difference in energy needs throughout the year. The energy need during summer is about 10% of the energy need in the winter. The reason for this difference is the heating system that keeps the building on a steady temperature of five degrees Celsius inside. The exact energy is therefore difficult to cover with a hybrid system.

For this specific situation of Valsörarna there is a big energy need during the winter and a significant smaller need during the summer. A hybrid system on this island is superfluous. As there is not much solar insulation during the winter, our decision was to use just a wind turbine. During the winter months the wind speed average is approximately 2 m/s per second higher than in the summer months.

The chosen device for Valsörarna is a wind turbine with an output of 10 kW. The manufacturer is Anhui Hummer Dynamo Co. LTD, and the model of wind turbine is H8.0 10kW. This system has been chosen because it is a system that supplies more electricity during the winter than during the summer, which is what the island needs. The complete datasheet of this wind turbine is found in *Appendix 14, Wind Turbine Datasheet*.

The data of wind speed averages and the power curve of the wind turbine are used to calculate the Power Out of the turbine. In the summer months the energy output of the wind turbine is about 2 kW and during the winter the energy output is around 4.8 kW. During the summer months the systems generate more energy than needed. However, a smaller wind turbine would not satisfy the needs during the winter months.

The price of this wind turbine depends on the type of installation. The total price with a single-phase converter is 12634,45. The price with a three phase converter is 13178,98. Transportation costs from Shanghai to Helsinki are 196,09. The detailed budget of the wind turbine and transportation is found in *Chapter 6.1.3, Mickelsörarna.*
Secondary system

The secondary system solution for Valsörarna is the same as for Mickelsörarna. Detailed information can be found in *Chapter 6.1.3, Mickelsörarna*.

Heating & Ventilation

The **heating** system that is used on Valsörarna is identical to the one used on Mickelsörarna *Chapter 6.1.3, Mickelsörarna/Heating& Ventilation*.

The **ventilation** of the building is also an exhaust ventilation system, like in the building on Mickelsörarna. The systems differ in two ways. The first is that every room contains its duct and ventilation tube, not only the kitchen, bathrooms and storage rooms. The other way is the penetration of the fresh air inside the building. The windows permit the air to pass through the specially built window jamb (for the technical drawing see *Appendix 5: Window Ventilation*). There is also inevitably air coming through cracks, small holes and openings around doors. The blueprints of the ventilation can be found in Appendix 05: Blueprints Valsörarna.

The figure below shows the heating and ventilation solution for Valsörarna (Figure 59).



Figure 59: Heating and ventilation solution for Valsörarna

A summary of the used heating and ventilation equipment for Valsörarna is shown in *Table 35* below.

		Valsöra	irna	
		Total area		760 m²
Building		Total volume		1864 m³
		Heating deman	d	10 kW
			Heat source	Ground
			Droprotios	Vertical
			Propreties	Closed loop
			Manufacterer	Gebwell Ltd.
	Host	numn	Туре	Gebwell T10
	Пеаг	pump	Heating output	10kW
			СОР	3
Heating			Power	3,3kW
			Borehole depth	120m
			Pipe length	240m
			Volume	2000
	Heat storage	Accumulator	Contents	Water-glycol (30%)
			Back-up resistor	6
	Exhaust he	at recovery	Heat source	Fuel cell
	Heat	output	Radiators	45°C/30°C
	Air s	upply	Natural	through the windows
		աթթւջ	Naturai	Cracks in the walls
			Ducts	1/room
Ventilation			Fans	6
Ventilation	Exhaust air	Mechanical	Pipes	6 types
			Moist control	
			Clock system	2h/day
		Heat recovery	,	/

Table 35: Data of heating and ventilation solution for Valsörarna

6.2 Summary

Table 36 is an overview of all the components of the four concept solutions. The chosen components are most suitable for each solution.

	GENERIC small	GENERIC bigger	MICKELSÖRARNA	VALSÖRARNA
Heat need	< 6 kW	6 to 10 kW	5.7 kW	10 kW
Electrical appliances	1.5 kW (estimation)	1.5 kW (estimation)	3.3 kW	0.5 kW (calc. with 1.5)
POWER NEED*	<3.5kW	3.5 to 5 kW	4.4 kW	5 kW
WIND TURBINE	Anhui Hummer Dynamo H8.0 10 kW	Anhui Hummer Dynamo H8.0 10 kW	Anhui Hummer Dynamo H8.0 10 kW	Anhui Hummer Dynamo H8.0 10 kW
SOLAR PANELS	Xuzhou Aibo Energy Tec. AB200M 30x200W=6 kW	Xuzhou Aibo Energy Tec. AB200M 60x200=12 kW	Xuzhou Aibo Energy Tec. AB200M 60x200W=12 kW	Not necessary
ELECTROLYZER	Acta AES200 200 l/h H ₂ @ 30 bar 1060 W input	Acta AES200 200 l/h H ₂ @ 30 bar 1060 W input	Acta AES200 200 l/h H ₂ @ 30 bar 1060 W input	Acta AES200 200 l/h H ₂ @ 30 bar 1060 W input
STORAGE	<15,000 l gas H ₂ @ 30 bar	15,000-20,000 l gas H ₂ @ 30 bar	~20,000 l gas H ₂ @ 30 bar	~20,000 l gas H ₂ @ 30 bar
FUEL CELL	ReliOn T-2000® 4kW Outdoor Config. (0 to 4 kW) 24/48VDC	Dantherm DBX5000 5 kW ,48 VDC	Dantherm DBX5000 5 kW ,48 VDC	Dantherm DBX5000 5 kW ,48 VDC
HEAT PUMP Ground Source, Closed Loop	Gebwell T6 2kW + accumulator (1000l) + EHR	Gebwell T10 3.3 kW + accumulator + EHR	Gebwell T10 3.3 kW + accumulator (2000l) + EHR	Gebwell T10 3.3 kW + accumulator + EHR
VENTILATION	(1 kW) Supply pipes & Exhaust pipes + HR + moist control + timer	(2 kW) Supply pipes & Exhaust pipes + HR + moist control + timer	(1 kW) Existing System + moist control + timer	(1 kW) Existing System + moist control + timer
Emergengy GENERATOR	Telgenco quiet48-5 (5kw – 48 VDC)	Telgenco quiet48-5 (5kw – 48 VDC)	Telgenco quiet48-5 (5kw – 48 VDC)	Telgenco quiet48-5 (5kw – 48 VDC)

Table 36: Final product choices

7 Discussion

7.1 Evaluation

The goal of this EPS project was to generate a sustainable and mostly autonomous solution for buildings in the Kvarken archipelago. The result of this project is a concept solution based on wind and solar energy, where excess energy is stored via hydrogen and converted into electricity when the wind and solar energy is not sufficient. The generated electricity can then be used to power the heating system, the ventilation system and the different appliances in the buildings.

The data given to the project team, by the project manager was not sufficient to make a fully specified and detailed solution. The result is as correct as possible, but at some stages there is a level of assumption. These assumptions are taken into account in the calculations made to determine the type and size of the chosen installations. It is possible that the presented solution may be oversized. It is oversized since in this project it is better to have an oversized system than an undersized system.

7.2 Validity

In this project there were some aspects that had to be estimated. Therefore, it is possible that the validity is a bit off. The estimations were made in a way that the system would not fail. E.g. the calculations are sized in a way that the system will definitely not be undersized and therefore not usable.

7.3 Reliability

The results of this project are reliable. The work methodology is used correctly; experts checked the results and the goals are achieved. The Energy Evaluation Model is designed and used as input for the concept. Where possible, the data has been double-checked. Data was available from Mickelsörarna; this data is used to check the reliability of the Energy Evaluation Model. The data calculated with the Energy Evaluation Model is accurate compared to the given data. The model also provided the data that was used in the calculations on Valsörarna, which means that the calculations were right. However, assumptions had to be made about the amount of working hours of the electric appliances.

7.4 Future

This project contained two main goals. The first objective was to make a model to estimate the energy needs. The second objective was to design a concept solution for Mickelsörarna, Valsörarna and similar remote off grid buildings in the archipelago. The output of this project is an Energy Evaluation Model and a concept solution. The Energy Evaluation Model is a tool made for engineers to make a fast estimation of the heating and electricity needs. The concept solution can be used as input for sustainable solutions in the Kvarken Archipelago near Vasa, Finland. Further research about piping, wiring and the control system is needed to make this concept solution in reality. It is however useful to use this project as input for similar projects.

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1 The Project

1.1 Appendix 01: Ekenäs Fair Posters

What

The goal of this European Project Semester is to provide sustainable energy for buildings on the Kvarken achipelago. The islands contain several and naturestations that have a certain demand of electricity and heating. The EPS team investigate generic solution for the islands energy demands.

Kvarken is part of the UNESCO's World Heritage



Buildings on Mickelsörarna

Why

In the winter the buildings need heating to handle the cold and the humidity. In the summer there is a higher energy need compared to the winter due to the visitors. Currently the stations energy is provided by fuel consuming methods that are not nature friendly. Finding sustainable alternatives solves this issue.

KVARKEN

How

NOVIA

WAR AND AND AND A MER'S.

Nowadays there are many different possibilities for sustainable energy. Finding the best suitable solution using the advantages of the archipelage is the challenge. By comparing all the possible alternatives, a final concept will be generated that can be applied on any designated island.

Sustainable Energy Solutions For the Kvarken archipelago



Figure 1: Poster Ekenäs Fair 01

Matrix

The matrix on the right is a compilation of the most suitable energy and heating solutions. All these sustainable solutions are chosen based on the available energy sources on the islands. The possibilities can be combined into different concepts. Each concept is a consistent system that will fulfill the energy demand at any time.





Concept



Figure 2: Poster Ekenäs Fair 02

HEAT

1.2 Appendix 02: Business Card



Figure 3: Business Card

2 Energy Demands

2.1 Appendix 03: Instruction Manual Electricity Evaluation

INSTRUCTIONS

*Fill the white cells, rest cannot be modified

Start:

Make a list of all appliances. Make sure AC (ALTERNATE CURRENT) and DC (DIRECT CURRENT) are separated.

Fill in the quantity of each appliance and the Power (Watts) (1 Kw = 1000Watts). Fill in the quantity of the appliances running during SUMMER and during WINTER. (i.e. If a heating device is only used during winter fill in a 0 in quantity in SUMMER and a 1 in WINTER)

Fill in the average amount of Hours per Day the appliance is used during SUMMER and WINTER.

The Summary below the table shows a rough calculation about

- The Average Consumption DC in kWhrs/h
- The Peak Consumption DC in kW
- The Average Consumption AC in kWhrs/h
- The **Peak** Consumption **AC** in kW
- The size of the **Inverter** needed (DC/AC)

Storing energy in an off-grid installation is useful for days when the primary energy source is not sufficient. This model provides two calculation models for storing energy.

The first is a battery bank. Fill in the **Voltage** (DC) of the system, the **Hours** of energy storage, the **Efficiency** and the **Maximum discharge** of the batteries. The model will calculate the **Estimated Size of the Battery Bank**

48	V
72	Hours
80%	%
70%	%
0,00	Ah
	48 72 80% 70%

When you choose to use a Fuel Cell as a storage device, fill the efficiency of the fuel cell (usually between 40% en 50%). Fill in the STP (*Standardized Temperature Pressure*) (usually between 3.2 and 3.5) and fill at what pressure the hydrogen in to be stored. The Model will calculate the:

- Total Back up Energy in kWhrs
- Total energy from H₂ in kWhrs
- H₂ Needs in Liters STP
- Estimated Size of the Hydrogen storage tank

essure in Bars	30	Bar
ergy Density of H ₂ (STP)	3,5	STP
ficiency	40%	%
tal Back up Energy	0,00	KWhrs
tal energy from H ₂	0,00	KWhrs
2 needs	0,00	Liters STP
. Size of Hydrogen Storage Tank ²	0,00	Liters
tal Back up Energy tal energy from H ₂ a needs Size of Hydrogen Storage Tank²	0,00 0,00 0,00 0,00	KWhrs KWhrs Liters S

2.2 Appendix 04: Instruction Manual Heating Evaluation

INSTRUCTIONS

*Fill the blank cells. Rest of cells cannot be modified.

Introduce:

- Outside minimum average temperature [in Celsius degrees].
- Ground minimum average temperature (approximate) [in Celsius degrees].
- Inside objective temperature [in Celsius degrees].
- Approximate **Volume** of building [in m³].
- Air changes per hour (see table on the bottom).
- Air Heat Recovery System **Efficiency**. If there is none, write 0 (zero) [in %].

Then start entering **surfaces data**, the *Thermal Resistance R* and *Thermal Transmittance U* values will appear once the *Material* is chosen. In case the material is not listed, the R and U values can be manually changed [R in $(m^2 \cdot K/W)$] [U in $(W/m^2 \cdot K)$].

Outside Wall i: enter the wall's surface [in m²]. You can choose 4 materials for each wall (different or repeated), if you don't need 4, leave the *Material* cell empty and write 0 (zero) as the R value for the ones you don't need.

Windows & Doors in Wall i: enter the surface to subtract from that wall that is occupied by windows or doors [in m²]. If there's no doors or windows in that wall, leave the *Material* cell empty and write 0 (zero) as the R value for the ones you don't need.

Roof i: enter the roof's surface from the plane view [in m²], a correction factor (1.15 for 30 degrees is defect, but you can change it) will be applied to take in account the pitch. Enter the material of the roof. The roof surface can be divided in 2 if there are 2 different types of roof. If there's only 1 type of roof, write 0 (zero) in the *Area* cell, leave the *Material* cell empty and write 0 (zero) as the U value for the second roof type.

Floor: enter the floor's surface [in m^2], then enter the material of the floor.

Window Type i: enter the surface for each window [in m^2] for that type. Then enter the material of that type of window. You can divide the total amount of windows in 4 different types. If there are not 4 different types, write 0 (zero) in the *Area* cell, leave the *Material* cell empty and write 0 (zero) as the U value for the window types that are not necessary.

Number of type i windows: enter the amount of windows of that type (same area, same material).

Door Type i: enter the surface for each door $[in m^2]$ for that type. Then enter the material of that type of door. If there is just one type of door, write 0 (zero) in the *Area* cell, leave the *Material* cell empty and write 0 (zero) as the U value for the second door type.

Number of type i doors: enter the amount of doors of that type (same area, same material).

Check that in the column HEAT LOSS due to TRANSMISSION there is not anything that is not a number. If there is something different to a number, please check the steps above again.

The materials table can be modified with new R or U values. Also with new materials; however, if that happens the formulas for columns Materials, Thermal Resistance and Thermal Transmittance must be modified as well. You will need the password for that.

RESULTS

In the TOTAL HEAT LOSS due to TRANSMISSION H_T

column you will find the amount of heat loss through the surfaces in Watts.

In the HEAT LOSS due to VENTILATION $\rm H_{v}$ column you will find the amount of heat loss for the air changes in Watts.

In the **GLOBAL U FOR THE BUILDING** (orange cells in the center) you will find the overall U value in $W/m^2 \cdot K$ for the building being studied. That will give an idea of how well insulated the building is.



In the **TOTAL HEAT LOSS** (red cells on the bottom and on the top right) you will find the total amoun of heat loss of the building according to the data introduced in Watts.



GLOSSARY

- ^⁰C degrees Celsius
- K degrees Kelvin
- W Watts (1 kilowatt (kW) = 1000 Watts (W))
- B Heat Recovery System Efficiency (%)
- V volume of the building
- N number of air changes per hour
- R_i thermal resistance R=1/U
- U_i thermal transmittance U=1/R
- $\Delta_{Temp} \quad temperature \, gap$
- H_T heat loss due to transmission (W)
- H_v heat loss due to ventilation (W)



2.3.1 Blueprint: Window Ventilation



2.3.2 Blueprint: Floor materials



RAK	(ENT	TEET	
AP	1	100 50 200	pintakäsittely teräsbet. styrox R, 1m ulkas. 50 +50 tiivistetty sora
VP	1	30 170 50	pintamateriaali pitabetoni teräsbetonilaatta min, villa
VP	3	22 19 13	pintamateriaali pontattu lastulevy puukannattajat, k 400, min.villa 100 rimoitus k 400 gyproc-levy, pintakäsittely
ΥP	1	23 30 250 0,2 45 13	huopakate 1k D raakapontti 23 x 95 tehdasvalm. kattoristikot k 900 tuuletettu ullakkotila tuulensuojalevy min.villa, 2 x 125 muovikelmu rimoitus k 400 gyproc-levy pintakäsittely
US	1	300 45 0,2 10	pintakäsittely sementtilaastirappaus kavytsoraharkkomuuraus koolaus, min.villa muovikelmu luja-levy, uralistakiinnitys
U5	3	44 22 12 50 120 120 13	pystylomalaudoitus, 22 + 22 rimoitus bituliitti vaskasoirot, min.villa rurko 120 x 50 k 600, min villa muovikelmu gyproc-levy pintakäsittely
¥5	1	13 90 13	pintakäsittely gyproc-levy runko 90 x 45 k 600, min.villa 70 gyproc-levy pintakäsittely
VS	2	130	pintakäsittely NKH muuraus pintakäsittely
VS	3	150	pintakäsittely teräsbetoni pintakäsittely

2.3.1 Blueprint Pipe types and Airflow



		PAAPIIRUSTUS 7(8)	001:1 VERNISINING	ARK 82-10 -07
	JAKOKUNIAN EBUSKARIN SAARI	LISÄRAKENNUS	MV-ASEMA, VALASSAARET BJÖRKÖBY MUSTASAARI	A STATE AND A STATE AND A STATE A STATE AND A STATE AN
7				
KOILUSEEN			NE	

2.3.3 Blueprint Building Valsorärna







5		
JAHOHUNNAN BJÖRKOBY YHT. ALUE (E885KÄR IN SAARI	•	
LISÄRAKENNUS	PÄÄPIIRUSTUS	
MV-ASEMA, VALASSAARET BJÖRKÖBY MUSTASAARI	POHJAPIIR ROS KELLARI	1:

2.3.5 Blueprint First Floor



JAKOKUNNAN BJÖRKÖBY, YHTEINEN ALUE, EBBSKÄRIN SAARI	*	
LISÄRAKENNUS	PÄÄPIIRUSTUS	3(
MV-ASEMA, VALASSAARET BJÖRKÖBY MUSTASAARI	POHJA PURROS 1. KERROS	1 : 10



7 JAKOKUNNAN BJÖRKÖBY, VHT. ALUE , EBBSKÄRIN SAARI LISÄRAKENNUS PÄÄPIIRUSTUS 4(8) 1:100 MV-ASEMA, VALASSAARET POHJAPIIRROS BJÖRKÖBY 2. KERROS MUSTASAARI AREXITERTINGTHONYO SALMINEN JA VÄRÄLÄ OF Sansbergininen 32 A1 SQUOD Setelakt 10 p. 546004 11.82 - Anile ARK 82-103-04

2.3.7 Blueprint Guard Tower


JAKOKUNNAN BJÖRKÖBY, YHT ALUE , EBBSKÄRIN SAARI		
LISÄRAKENNUS	PÄÄPIIRUSTUS	5(8)
MV-ASEMA, VALAS SAARET BJÖRKÖBY MUSTASAARI	POHJAPIIRROKSET PÄIVYSTYSTASO ULLAKKO	1 : 100



2.3.9 Blueprint Construction Details 2

Rakennuskohde Mv-asema, Valassaaret Rakennetyypin nimi Välipohja	7 10	Työn numero ⁸ Rakennetyypin 2254 VP 1,	tunnus VP 2
Rakennetyypin kuvaus (piirros ja selostus)	Mittakaava 1:10		- 11
VP 1	- - 30 mm	pintamateriaali teräshiottu betoni	arkk.
	- 170 mm - 100 mm	teräsbetonilaatta akustiikkalevy TA-100	rak.
Juning		$k = 0,42 W/m^{20}C$ $I_{i} = 63 dB$ $I_{a} = 57 dB$	×.
VP 2	- 10 mm - 20 mm - 30 mm	lattialaatat kiinnityslaasti, sem: suojabetoni K 20 2 3-150	arkk.
	- - 40 mm	vedeneristys RT 83-10153 olosuhderyhmä 2 teräshiottu betoni	rak.
	- 170 mm - 100 mm	teräsbetonilaatta akustiikkalevy TA-100	rak.
		$k = 0,42 \text{ W/m}^{20}\text{C}$ T = 63 AFF	



2.3.10 Blueprint Construction Details 3



2.3.11 Blueprint Construction Details 4



2.3.12 Blueprint Constructions Details 5

Leatija m m	2	Hyváka	yjā	\$	Paixays		Sivu	⁵ Muuto
Rakennuskohde				7	11.1.1985 Tyon numero	8	Bakennetw	nin hunnus
Mv-asema, Va	lass	aare	et		2254		112	A
Ulkoseinä				10	22/4		05	*
Rekensetyvnin kuveur (ni	inten la	nalost	unl .	Ministeres				
nakerineryypin kuraus (pi	eros ja	seroan	18)	1.10				
				1110				
US 4								
	۰.			minerit-1	evy) pofs	tetao		
	-			kattohuon	a point	40 400		
	-	22	mm	harvalaud	oitus /			
TUNKA	_			tervapapa	ri			
)			
	1			pintakäsi	ttelv) list	****
BB	-	22	+22	mm pystyl	omalaudoitus		1	
TIRKI		22	mm	rimoitus	22 x 100 k 12	200	1	
	-	12	mm	bituliitt	i		T	
	-	50	=	vaakasoir	ot 50 x 50 k	600	+]	
				mineraali	villa 01.045		J	
	-	22	mm	laudoitus	22 x 100			
	-			tervapape	ri			
	-	100	mm	pystyrunk	0 100 x 50 k	600 -	2	
				mineraali	222			
					villa 01.045			
	-			pahvi	villa 01.045			
	-	19	mm	pah v i ponttilau	villa 01.045 ta			
		19 12		pahvi ponttilau lastulevy	villa 01.045 ta			

2.3.13 Blueprint Construction Details 6

2.3.14 Blueprint Construction Details 7



SOURCE: (Senate Fastigheter, Vaasan yliopisto, Vaasa, Finland.)

2.4 Appendix 06: Blueprint Mickelsorärna

2.4.1 Blueprint Mickelsorärna 1



2.4.2 Blueprint Mickelsorärna 2



UUDISRAKENNUS	PÄÄPIIRUSTUS	
MIKKELINSAARTEN MERIVARTIOASEMA 65800 RAIPPALUOTO	JULKISIVUT POHJOISEEN	٨٢
8205-1/07		1:100
ARKKITEHTITDIMISTO ALW-ARK OY KIRKKOPUISTIKKO 5A3 65100 VAASA 10 PUH 961-112729 Multure 10.05.85	ARK 38-010	1



MAKSAMAA - KUMM	ELSKAR - 7		
UUDISRAKENNUS		ALAKATTOPIIRUSTUS	
MIKKELINSAARTEN MERIVARTIOASEMA 65800 RAIPPALUOTO) 8205-1/07	POHJAPIIRUSTUS 2. KERROS	1:50
ARKKITEHTITOIMISTO ALW-ARK OY KIRKKOPUISTIKKO SA3	PUH 961-112729 65100 VAASA 01 11 85	ARK 38-503	

2.4.4 Blueprint Mickelsorärna 4



MAKSAMAA - KUMMELSKAR-7	
UUDISRAKENNUS	ALAKATTOPURUSTUS
MIKKELINSAARTEN MERIVARTIOASEMA 65800 RAIPPALUOTO 8205 -1/07	KELLARIKERROS
АRKK/TENT/TOMESTO AUW-ARK OY PUH 961-02729 К/ЯНКОРUSTIKKO 3-A3 65500 VAASA 0117 85	ARK 38- 501

SOURCE: (Forest Department, Building B13 Yliopistonranta, Vaasa, Finland.)

2.5 Appendix 07: Weather Data

	P _{air} (hPa)		air	temp. (≌C)			xtreme	temp. (^g	2 C)		temperature days				
		0 UTC	6 UTC	12 UTC	18 UTC	mean	avg. Max	avg. Min	absol. max	year	absol. Min	year	Max <25	Max <0	Min <0	Min <- 10
jan	1007	-4,6	-4,6	-4,3	-4,4	-4,5	-2,3	-6,9	6,4	1991	- 27,8	1986	-	17	28	8
feb	1010	-5,7	-6,1	-4,9	-5,3	-5,5	-3,2	-8,1	5,6	1992	- 27,2	1985	-	18	26	10
mar	1010	-3,7	-4,1	-1,9	-2,9	-3,1	-0,7	-5,7	7,3	2004	- 23,2	1987	-	15	28	7
apr	1013	0,1	0,5	2,4	1,2	1	3,6	-1,1	16,6	2002	-14	1985	-	3	18	0
may	1014	4,6	5,7	7,4	6,3	6	9,1	3,5	21,5	1992	-4,5	1981	-	0	2	-
jun	1011	9,6	10,8	12,5	11,6	11,1	14,1	8,7	25,3	1989	1,5	1985	0	-	-	-
jul	1011	13,9	14,9	16,6	15,7	15,3	17,9	13	27,5	2003	6,6	2008	0	-	-	-
aug	1011	14	14,4	16,2	15,2	14,9	17,3	12,9	26	2006	5,6	1986	0	-	-	-
sep	1011	10,1	9,9	11,7	10,6	10,6	12,7	8,7	22	2002	0,7	1986	-	-	-	-
oct	1010	5,6	5,4	6,4	5,8	5 <i>,</i> 8	7,4	4,2	15	2000	-8	1992	-	0	3	-
nov	1009	1,2	1,1	1,4	1,2	1,2	2,8	-0,5	9,5	1999	- 15,6	2002	-	5	16	0
dec	1008	-2	-2,1	-1,9	-1,9	-2	-0,1	-4	7	2000	- 22,6	1985	-	13	23	4
AVG.	1010	3,6	3,8	5,1	4,4	4,2	6,6	2,1	27,5		- 27,8		0	71	144	29

Table 1: Air Temperature, Extreme Temperatures And Days

(Tilastoja Suomen ilmastosta 1981-2010. Finnish Meteorological Institute., 2012)





Figure 4: Air Temperature Graph

Table 2: Relative Humidity And Precipitation

		relati	ive hu	midity	%					precipitation mm									
		time	UTC								рі	ecipita	tion da	ays	snow depth cm				
	0	6	12	18	mean	mean	max	year	min	year	>=0,1m m	>=1m m	>=10m m	daily prec.	first to 15th	15th to last			
1	87	87	86	86	87	39	74,5	1990	9,5	1996	19	10	0	18,9	18	23			
2	87	88	85	87	87	30	62,3	1999	1,3	1994	14	7	0	16,9	25	29			
3	88	89	83	87	87	31	55,8	2008	8	2005	14	8	0	19,9	33	29			
4	86	84	77	82	82	22	65,4	2000	1,3	2002	10	5	0	23,5	19	9			
5	85	81	72	77	79	32	72,5	1982	3,6	1994	10	6	1	23,5	1	-			
6	86	81	73	76	79	39	98,6	1981	0,4	1982	10	6	1	37,6	-	-			
7	87	82	74	79	81	51	134,3	2008	2	1994	11	7	2	59,9	-	-			
8	86	83	75	79	81	54	92,9	1985	12,5	1994	13	8	2	42,1	-	-			
9	84	85	76	81	82	49	103,8	1992	10,9	2008	13	8	1	44,2	-	-			
10	84	84	80	82	83	54	103,3	2006	13,2	2005	16	10	1	25,7	1	1			
11	85	86	84	84	85	53	104,6	1996	10,2	1993	18	10	1	24,4	1	5			
12	87	87	86	86	87	43	89,7	1993	10,7	2002	18	10	1	23,7	5	13			
	86	85	79	82	83	497	134,3		0,4		166	95	10	59,9					

(Tilastoja Suomen ilmastosta 1981-2010. Finnish Meteorological Institute. , 2012)

Table 3: Sunshine %

Month	Sunshine %
jan	0,18
feb	0,3
apr	0,37
mar	0,44
may	0,51
jun	0,51
jul	0,49
aug	0,45
sep	0,35
oct	0,29
nov	0,2
dec	0.15

(Chinci Word Atlas, 2011)





Average rain days, frost days, precipitation and sunshine % over the last 20 years in Mikkelinsaaret, Western Finland, Finland (islands).

Figure 5: Sunshine %

Table 4: Wind Distribution

									wind d	istribu	ition							
	N		NE		E		SE		S		SW		w		NW		calm	mean
	m/s	%	m/s	%	m/s	%	m/s	%	m/s	%	m/s	%	m/s	%	m/s	%		
1	8,6	13	7,4	8	6	8	4,7	14	6,9	19	7,5	15	7,1	13	7,3	10	1	6,8
2	7,9	10	7,4	11	5,2	8	4,2	12	6,8	22	6,9	16	6,5	12	6,5	7	1	6,2
3	7,5	12	6,6	11	4,6	8	4,3	9	6,8	27	5,7	15	6	10	5,9	7	1	5,7
4	7,1	12	6,5	17	4,3	8	3,8	6	6,2	25	5,2	14	5,4	10	5,5	6	1	5,3
5	5,9	12	6	19	4	8	3,6	3	6	24	5	17	5	10	4,9	7	0	4,9
6	5,7	13	5,6	19	3,8	9	3	4	6	21	4,8	16	4,7	10	4,9	8	1	4,7
7	5,7	11	5,5	16	3,8	8	3,3	6	5,4	22	4,7	17	4,8	10	5	8	1	4,6
8	6,6	12	6,2	16	4,6	9	3,6	8	5,2	19	4,9	17	5,4	10	5,8	8	1	5,1
9	7,4	11	6,7	11	5	8	3,8	10	5,7	20	5,9	16	6,8	13	7,2	11	1	5,9
10	8,8	12	7,5	7	6,8	7	4,7	13	6,9	20	7	18	7,5	13	7,8	9	1	7
11	8,9	12	8,6	7	7,2	8	5	16	6,8	18	8	16	7,6	12	7,7	10	1	7,4
12	8,7	12	9,1	7	6,8	7	4,6	15	7	18	7,6	15	7,6	14	8	12	0	7,2
	7,3	12	6,9	12	5,2	8	4,1	10	6,3	21	6,1	16	6,2	11	6,4	8	1	5,9

(Tilastoja Suomen ilmastosta 1981-2010. Finnish Meteorological Institute., 2012)

Table 5: Wind Speed and Direction (During Winter months)

nov. to apr	N	NE	E	SE	S	sw	w	NW		avg
	m/s	m/s	m/s	m/s	m/s	m/s	m/s	m/s		
11	8,9	8,6	7,2	5	6,8	8	7,6	7,7		7,475
12	8,7	9,1	6,8	4,6	7	7,6	7,6	8		7,425
1	8,6	7,4	6	4,7	6,9	7,5	7,1	7,3		6,9375
2	7,9	7,4	5,2	4,2	6,8	6,9	6,5	6,5		6,425
3	7,5	6,6	4,6	4,3	6,8	5,7	6	5,9		5,925
4	7,1	6,5	4,3	3,8	6,2	5,2	5,4	5,5		5,5
AVG	8,11666667	7,6	5,68333333	4,43333333	6,75	6,81666667	6,7	6,81666667	6,61458333	

(Tilastoja Suomen ilmastosta 1981-2010. Finnish Meteorological Institute., 2012)

Table 6: Wind Distribution (During Winter months)

nov. to apr	N	NE	E	SE	S	SW	W	NW
	%	%	%	%	%	%	%	%
11	12	7	8	16	18	16	12	10
12	12	7	7	15	18	15	14	12
1	13	8	8	14	19	15	13	10
2	10	11	8	12	22	16	12	7
3	12	11	8	9	27	15	10	7
4	12	17	8	6	25	14	10	6
AVG	11,833333 3	10,166666 7	7,8333333 3	12	21,5	15,166666 7	11,833333 3	8,666667

(Tilastoja Suomen ilmastosta 1981-2010. Finnish Meteorological Institute., 2012)



Figure 6: Wind Speed, Distribution and Direction

(Tilastoja Suomen ilmastosta 1981-2010. Finnish Meteorological Institute., 2012)



Figure 7: Wind Speed and Average

(Tilastoja Suomen ilmastosta 1981-2010. Finnish Meteorological Institute., 2012)

2.6 Appendix 08: Mickelsörarna Electricity Needs

AC APPLIANCES

ALTERNATE CURRENT	(AC)	SUMMER					w	INTER	WINTER			
Appliance Name	Power (W)	Quantity Summer	Total (W)	Hrs/day	W/hrs per day	AVG Load	Quantity Winter	Total (W)	Hrs/day	W/hrs per day	AVG Load	
Technical Fac.			0		0,00	0,00		0		0,00	0,00	
Heatng wtr pump	100	1	100	4	400,00	16,67	2	200	2	400,00	16,67	
Fuel Pump	75	1	75	2	150,00	6,25	1	75	4	300,00	12,50	
Elec. Burner	90	1	90	4	360,00	15,00	1	90	7	630,00	26,25	
Water pump	80	1	80	7	560,00	23,33	1	80	2	160,00	6,67	
oil pump	55	1	55	2	110,00	4,58	1	55	24	1320,00	55,00	
rmt cntrl	6	1	6	24	144,00	6,00		0		0,00	0,00	
used water pump	2000	1	2000	2	4000,00	166,67		0		0,00	0,00	
			0		0,00	0,00		0		0,00	0,00	
Kitchen			0		0,00	0,00		0		0,00	0,00	
Fan	50	1	50	8	400,00	16,67		0		0,00	0,00	
Microwave	800	1	800	4	3200,00	133,33		0		0,00	0,00	
coffee maker	750	1	750	2	1500,00	62,50		0		0,00	0,00	
refrigerator	200	1	200	24	4800,00	200,00		0		0,00	0,00	
freezer	200	1	200	24	4800,00	200,00		0		0,00	0,00	
dishwasher	2000	1	2000	2	4000,00	166,67		0		0,00	0,00	
Drying Room fan	90	1	90	3	270,00	11,25		0		0,00	0,00	
			0		0,00	0,00		0		0,00	0,00	
Heating System			0		0,00	0,00		0		0,00	0,00	
Nw Heating system	3300	1	3300	0	0,00	0,00	1	3300	24	79200,00	3300,00	
			0		0,00	0,00		0		0,00	0,00	
			0		0,00	0,00		0		0,00	0,00	
			0		0,00	0,00		0		0,00	0,00	
Observation Tower	144	1	144	5	720,00	30,00		0		0,00	0,00	
exit lights	77	1	77	24	1848,00	77,00		0		0,00	0,00	
Lighting	1020	1	1020	12	12240,00	510,00		0		0,00	0,00	
Technical Fac.	436	1	436	4	1744,00	72,67		0		0,00	0,00	
outdoor lighting	240	1	240	5	1200,00	50,00		0		0,00	0,00	
			0		0,00	0,00		0		0,00	0,00	
Mobile Phone	1580	1	1580	24	37920,00	1580,00	1	1580	24	37920,00	1580,00	
			0		0,00	0,00		0		0,00	0,00	
Total AC Consumption	on		13293		80366	3348,58		5380		119930	4997,08	

(Spreadsheet obtained from the Project Manager.)

DC APPLIANCES

DIRECT CURRENT (DC)		SUMMER							WINTE	R	
Appliance Name	Power (W)	Quantity Summer	Total (W)	Hrs/day	W/hrs per day	AVG Load	Quantity Winter	Total (W)	Hrs/day	W/hrs per day	AVG Load
			0		0,00	0,00		0		0,00	0,00
Heatng wtr pump	100	0	0	1	0,00	0,00	4	400	0	0,00	0,00
Fuel Pump	75	0	0		0,00	0,00	1	75	0	0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
Total DC consumption			0		0	0,00		475		0	0

RESULTS

TOTAL ELECTRICITY NEEDS	SUM	IMER	WINTER
AVERAGE AC CONSUMPTION	3,35	KWhr s/h	5,00 KWhrs/ h
PEAK AC CONSUMPTION	13,29	кw	5,38 KW
Inverter ((requires 10%	14.62	кw	Based on (MAX Total Load * 1,1)/1000
Energy (DC/AC))	_ ,,		(Inverter needs 10%)
AVERAGE DC CONSUMPTION	0,00	KWhr s/h	0,00 KWhrs/
PEAK DC CONSUMPTION	0,00	ĸw	0,00 KW
Voltage of DC System in V	48	v	
Number of Days Backup storage is required	72	Hour s	
System in %	80%	%	
Maximum Discharge in %	70%	%	
Est. Size of Energy Storage ¹ (Batttery Bank)	8566, 43	Ah	¹ Based on: ((<i>Max</i>)Total Load * Hours of Storage / Volt of DC system) / (Maximum Discharge * Efficiency)
Duran in			Source: http://www.solaronline.com.au
Bars	300	Bar	
Energy Density of H ₂ (STP)	3,5	STP	
Efficiency	45%	%	
Total Back up Energy (from H2)	359,7 9	KWhr s	Total Energy * Hrs of Back up
Total energy in H ₂	799,5	KWhr	Total Back up Energy / Efficiency
H ₂ needs	22843 8,10	Liters STP	Total power from $H_2 * 1000 / STP$
Est. Size of Hydrogen Storage Tank ²	761,4 6	Liters	² Based on: Liters STP / Pressure

2.7 Appendix 09: Valsörarna Electricity Needs

AC APPLIANCES

ALTERN	ATE (AC)		SI					•	WINTER		
Appliance	Power	Quantity	Total	Hrs/	W/hrs	AVG	Quantity	Total	Hrs/	W/hrs	AVG
Name	(W)	Summer	(W)	day	per day	Load	Winter	(W)	day	per day	Load
			0		0,00	0,00		0		0,00	0,00
Fans			0		0,00	0,00		0		0,00	0,00
Fan 1	400	1	400	1	400,00	16,67	1	400	1	400,00	16,67
Exhaust Fan 2	400	1	400	1	400,00	16,67	1	400	1	400,00	16,67
Exhaust Fan 3	300	1	300	1	300,00	12,50	1	300	1	300,00	12,50
Drying Fan 1	400	1	400	1	400,00	16,67	1	400	1	400,00	16,67
Exhaust Fan 4	400	1	400	1	400,00	16,67	1	400	1	400,00	16,67
Exhaust Fan 5	400	1	400	1	400,00	16,67	1	400	1	400,00	16,67
Exhaust Fan 6	400	1	400	24	9600,00	400,0 0	1	400	24	9600,00	400,0 0
			0		0,00	0,00		0		0,00	0,00
Pumps			0		0,00	0,00		0		0,00	0,00
Pump 1	300	1	300	0	0,00	0,00	1	300	18	5400,00	225,0 0
Pump 2	300	1	300		0,00	0,00	1	300	1	300,00	12,50
Pump 3	300	1	300		0,00	0,00	1	300	1	300,00	12,50
Pump 4	300	1	300		0,00	0,00	1	300	1	300,00	12,50
Pump 5	500	1	500		0,00	0,00	1	500	1	500,00	20,83
Pump 6	1500	1	1500		0,00	0,00	1	1500	1	1500,00	62,50
Pump 7	2500	0	0		0,00	0,00	1	2500	0	0,00	0,00
Pump 8	2500	0	0		0,00	0,00	1	2500	1	2500,00	104,1 7
Pump 9	3000	0	0		0,00	0,00	1	3000	1	3000,00	125,0 0
			0		0,00	0,00		0		0,00	0,00
Boiler	5000	0	0	0	0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
Small Purificatio n	2200	0	0	0	0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
Alarm Sensors	0	1	0	24	0,00	0,00	1	0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
Heat Pump	3300	1	3300	0	0,00	0,00	1	3300	24	79200,0 0	3300, 00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
			0		0,00	0,00		0		0,00	0,00
Total A Consump	AC otion		9200		11900	495,8 3		1720 0		104900	4370, 83

(Senate Fastigheter, Vaasan yliopisto, Vaasa, Finland.)

NO DC APPLIANCES

RESULTS

	_		
TOTAL ELECTRICITY NEEDS	SUN	IMER	WINTER
AVERAGE AC	0,50	KWhr	4,37 KWhrs/
CONSUMPTION PEAK AC		s/h	h
CONSUMPTION	9,20	ĸw	17,20 KW
Inverter ((requires 10% Energy (DC/AC))	10,12	кw	Based on (MAX Total Load * 1,1)/1000 (Inverter needs 10%)
AVERAGE DC	0,00	KWhr	0,00 KWhrs/
PEAK DC	0.00	s/n	n
CONSUMPTION	0,00	ĸw	0,00 KW
Voltage of DC			
System in V	48	v	
Number of Days Backup	72	Hour	
Efficiency of Back up		5	
System in %	80%	%	
Maximum Discharge in %	70%	%	
Est. Size of Energy Storage ¹	7492,	Ah	¹ Based on: ((<i>Max</i>)Total Load * Hours of Storage / Volt of DC
(Batttery Bank)	86		system) / (Maximum Discharge * Efficiency)
Pressure in			<u>Source. http://www.solatonine.com.au</u>
Bars	30	Bar	
Energy Density of H ₂ (STP)	3,5	STP	
Efficiency	40%	%	
Total Back up Energy	35,70	KWhr	Total Power * Hrs of Back up
		s KWhr	
Total energy from H ₂	89,25	s	Total Back up Power / Efficiency
H₂ needs	2550 0.00	Liters STP	Total power from H ₂ * 1000 / STP
	-,		
Est. Size of Hydrogen	850,0	Liters	² Based on: Liters STP/ Pressure
Storage Tank	0		

2.8 Appendix 10: Valsörarna Heat Needs

T inside	5		Т	OTAL HEAT LOSS		10044		Watts
T outside	-20							
Tground	0	area (m2)	type	U (W/m2.K)		heat loss		Total
WALLS	no data on t	he old building	g, will use	e * as U for those v	valls	*	0,25	2490,5125
NW	new	93,22	US 3	0,23		536,015		-
	old	28,68	?	0,25		179,25		
NE	new	57,645	US 3	0,23		331,4588		
	old	0	?	0,25		0		
SE	new	106,8	US 3	0,23		614,1		
	old	26,68	?	0,25		166,75		
SW	new	32,685	US 3	0,23		187,9388		
	old	30	?	0,25		187,5		
guard tower		46	B 30	0,25		287,5		
WINDOWS		small	0,36	medium	0,72	big	2,16	3744,290865
	triple gla	ss 0,418, air c	avity 0,18	8, single glass 0,02	6			
NW	new	17,28		1,60		692,3077		
	old	4,32		1,60		173,0769		
NE	new	6,48		1,60		259,6154		
	old	0		1,60		0		
SE	new	16,2		1,60		649,0385		
	old	4,32		1,60		173,0769		
	basement	2,88		1,60		115,3846		
SW	new	1,44		1,60		57,69231		
	old	0		1,60		0		
guard tower		40,54		1,60		1624,099		
tilt + corners correction factor	1,15							
DOORS								625
NW	new	12,5		1		312,5		
	old	0		1		0		
NE	new	10,5		1		262,5		
	old	0		1		0		
SE	new	0		1		0		
	old	2		1		50		
SW	new	0		1		0		
	old	0		1		0		
BASEMENT				hat an a haide			1.1.1	1446,51
about half of the wall under gro	und level, so v	vill take the av	vg. temp.	between outside	and gi	round to calcu	late th	e temp gap.
NW	type US 2	28,75		0,35		150,9375		
	type US 1	27,5		0,43		1/7,375		
	r turna LIC D	27,5		0,4		105		
INE .	type US 2	13,5		0,35		70,875		
SE	type US 1	17 5		0,43		01 975		
3E	type US 2	17,5 22.7E		0,35		91,075 217 6975		
	iype 03 I	35,75		0,45		217,0875		
510/	: 2	24,02		0,4		147,72		
300	ŗ	20		0,4		120		
floor	AP 1	196.8		0.31		305.04		
ROOF		/ -		-,-		/-		1118,9375
	new	159,75		0,17	*1	678,9375		
	ادلم	00		0.2	* 2	440		
	old	88		0,2	ΨZ	440		
	tower	0		0,17		0		
*1 no clear data, but will use the s	same value for	r both new roc	o <u>fs; *</u> 2 no	data, will use a vo	alue w	<u>vith less</u> isolati	on that	the new roof
VENTILATION								618,75
Heat recovery Efficiency (%)	β	50						
Air Changes per Hour	N	0,083333				C10 7F		
Volume of room or building (m3)	V	1800				010,/5		
Temperature difference (K)	Δ_{temp}	25						
						TOTAL		10044 Watts

3 Systems

3.1 Appendix 11: Secondary Power System

3.1.1 Hydrogen Production

There are different possibilities when it comes to H_2 production. This is a comparison of them and their main characteristics:

3.1.1.1 Hydrogen from FOSSIL FUELS

Production From Natural Gas

• Steam Reforming (steam methane reforming – SMR)

Endothermic conversion of methane and water vapor into hydrogen and carbon monoxide. Needs an external heat input Carbon monoxide can be further converted to carbon dioxide and hydrogen in a water-gas shift reaction.

 $CH_4 + H_2O + heat --> CO + 3H_2$ $CO + H_2O --> CO_2 + H_2 + heat$

• Partial Oxidation (POX)

Exothermic combustion of methane with oxygen to produce carbon monoxide and hydrogen. No need for any external heat input.

 $CH_4 + \frac{1}{2}O_2 --> CO + 2H_2 + heat$

• Auto-thermal reforming (ATR)

Combination of both- Total reaction is exothermic. Outlet 950 to 1100 °C and up to 100 bar. Gas purification rises costs and lowers global efficiency.

Production From Coal

Variety of existing gasification processes. Most favorable is high-temperature entrained flow process, because maximizes carbon conversion to gas and avoids accumulation of char, tars and phenols. Typical reaction, carbon becomes carbon monoxide and hydrogen. Requires heat input. Produced carbon monoxide is further converted to carbon dioxide and hydrogen through water-gas shift reaction. It's commercially available, but more complex than producing from natural gas. Cost of resulting hydrogen is higher, too.

Comparison Table 07:

Table 7: Comparison of hydrogen from Fossil Fuel systems

Technology	Natural Gas SMR	Natural Gas POX or ATR	Coal
Benefits	High efficiency Emissions Costs for large units	Smaller size Costs for small units Simple system Exothermic	Commercially mature Exothermic
Challenges	Complex system Sensitive to natural gas quality Endothermic	Lower efficiency H2 purification Emissions/flaring	Most complex system Resulting H2 cost

3.1.1.2 Hydrogen from SPLITTING OF WATER

Water Electrolysis

Water is split into hydrogen and oxygen using electrical energy.

• Alkaline electrolysis

Uses an aqueous caustic solution (KOH) as an electrolyte circulating through the cells, which are arranged in a stack. It is suitable for stationary applications, can operate with pressures up to 25 bar. It is a mature technology widely applied. Suitable for remote operation. Reactions that take place inside the alkaline electrolysis cell:

Electrolyte:	4H ₂ O> 4H ⁺ + 4OH ⁻
Cathode:	4H ⁺ + 4e> 2H ₂
Anode:	$40H^{-} - > O_2 + 2H_2O + 4e^{-}$
Sum:	2H ₂ O> O ₂ + 2H ₂

It is still a challenge to design and manufacture electrolyzing equipment with higher efficiency and larger turn-down ratios, at lower costs.

• Polymer electrolyte membrane (PEM) electrolysis

It requires no liquid electrolyte, which simplifies the design significantly. It uses an acid polymer membrane. Higher operation pressures of up to several hundred bars. It's suited for both stationary and mobile applications. Higher turndown ratio. No KOH electrolyte makes it safer. Higher densities allow them to have a more compact design.

Anode (oxidation):	$2 \text{ H}_2\text{O} \rightarrow \text{O}_2 + 4 \text{ H}^+ + 4\text{e}^-$	E ^o _{ox} = -1.23 V
Cathode (reduction):	2 H ⁺ + 2e ⁻ → H ₂	$E_{red}^{o} = 0.00 V$

The negative voltage in the oxidation of the anode means that the reaction needs energy to take place.

This could be simplified considering the electrolyzer as a whole, then:

Overall reaction: $2 H_2O(I) + Electricity (1.23 V) --> 2 H_2(g) + O_2(g)$

Not as mature technology as alkaline, due to relatively high cost, low capacity (enough for this project needs), not great efficiency (up to 60% for electricity, and up 85 for CPH). In the last years PEM technology and performance has improved significantly.

• High-temperature electrolysis

Electrical energy needed to split water at 1000°C is considerably lower that at 100°C (low-temp. electrolysis), therefore, significantly higher efficiencies can be achieved. Most extended technology is Solid Oxide Electrolyzer Cell (SOEC) based on a reversible Solid Oxide Fuel Cell (SOFC), operating at 700 to 1000°C, range in which electrode reactions are more reversible.

It's still a young technology. Current challenges relate to thermo-mechanical stress resistant materials development (same challenges as for the SOFC).

Comparison Table 08:

Table 8: Comparison of hydrogen from Splitting Water systems

Technology	Alkaline	PEM	High-temperature
Benefits	Suits stationary Up to 25 bar Remote operation	No liquid electrolyte Simple design High pressure Mobile & Stationary Large turn-down ratio Safer Small size (compact) Efficiency for CHP	Higher efficiency Reversible Fuel Cell
Challenges	Low efficiency Small turn-down ratio Cost	Evolving technology High cost Low capacity (enough) Efficiency for only electricity	Needs more R&D Materials

Photo-Electrolysis (Photolysis)

Electrolyzer coupled to a Photovoltaic system. It offers flexibility, the output can be used directly as electricity or to run the electrolyzer. Light is used to split water directly into hydrogen and oxygen. It has great potential for cost reduction of hydrogen production.

It still needs material and engineering systems R&D. efficiencies only up to 15-20%.

Photo-Biological Production (Biophotolysis)

Two steps: photosynthesis and hydrogen production catalyzed by hydrogenases, for example algae and cyanobacteria, or artificial photosynthesis

Photosynthesis:	$2H_2O> 4H^+ + 4e^- + O_2$
Hydrogen Production:	$4H^{+} + 4e^{>} 2H_{2}$

High-Temperature Decomposition

At a temperature of about 3000°C 10% of water is split, the remaining 90% can be recycled. To reduce operation temperatures, other processes can be used:

- Thermo-chemical cycles
- Hybrid systems coupling thermal and electrolytic decomposition
- Direct catalytic decomposition via a ceramic membrane
- Plasma-chemical decomposition in a double-stage CO2 cycle.

Up to 50% efficiencies can be expected for the aforementioned processes. There is still R&D to be done concerning corrosion resistant materials, heat exchangers, and heat storage, thou.

3.1.1.3 BIOMASS to Hydrogen

In biomass production, the gasses created contain hydrogen, in a manner similar to the gasification of coal. However, these gases are rarely used, due to the unrefined products with inconsistent quality of the biomass generation side products. Also, quite a big amount of biomass is needed in relation to the hydrogen production.

Hydrogen will be produced in an ELECTROLYZER, using pure water and electricity as inputs:

3.1.2 Choice: Pem Electrolyzer

Product	H₂prod. rate (l/h)	H ₂ pressure (bar)	H ₂ purity (%)	Power (kW)	Comments / Reasons for discarding
HOGEN GC 300	18	13.8	99.9999	<1	Low II flow rate data missing
HOGEN GC 600	36	13.8	99.9999	<2	LOW H ₂ now rate, data missing
HOGEN GC 4200	252	13.8	99.9999	3.2	Low H ₂ pressure, high power consumption
HOGEN HP 10	260	166	99.995	?	Data missing high processor
HOGEN HP 40	1050	166	99.995	?	Data missing, high pressure
HOGEN H2m	2000	16/31	99.9995	14.6	
HOGEN H4m	4000	16/31	99.9995	28	
HOGEN H6m	6000	16/31	99.9995	40.8	Consumed too much nower
HOGEN C10	10000	31	99.9998	62	Consumed too much power
HOGEN C20	20000	31	99.9998	120	
HOGEN C30	30000	31	99.9998	174	
Acta Energy AES100	100	15/30	99.999	0.53	
Acta Energy AES200	200	15/30	99.999	1.06	Suitable for the islands work
Acta Energy AES300S	300	15/30	99.999	1.59	at 30 bar, high H ₂ purity, low
Acta Energy AES300L	300	15/30	99.999	1.59	power consumption
Acta Energy AES500	500	15/30	99.999	2.65	
Acta Energy AES1000	1000	15/30	99.999	5.3	Consumed too much power
Electric Hydrogen HG02	200	14.7	99.90	1	Low H ₂ pressure

3.1.2.1 Different PEM electrolyzers (Table 09, Table 10)

Table 9: Comparison of PEM Electrolyzers

Table 10: PEM ELECTROLYZER choice for each application:

Application	Choice
Smaller needs concept (<=3.5 kW)	
Bigger needs conpcet (3.5 to 5 kW)	Acta Energy AES200
Mickelsörarna (4.4 kW)	Acta Energy AES200
Valsörarna (5kW)	

This device is suitable for all the different systems.

3.1.3 Hydrogen Storage

When it came to choose a storage type for hydrogen, the technical aspects that had to be taken in account were:

- Pressure
- Storage Size
- Temperature
- Reliability
- Safety
- Storage cost

Following there is an overview of the most common ways to store hydrogen, which were the ones that were looked into before a choice was made. The main characteristics of each of the systems are mentioned as well.

3.1.3.1 GASEOUS Hydrogen

<u>Metal Tanks</u>

Steel tanks are not the most suitable solution for hydrogen storage: the small size of hydrogen molecules makes it easy for them to escape through the metal when hydrogen is stored under a high pressure. Also they are very heavy in relation to the amount of pressure they can withstand. But those issues should not be a problem if the storage pressure is not great, and space availability is not critical. Also they are a lot less expensive than composite tanks.

Composite Tanks

Carbon fiber wrapped storage tanks can stand bigger pressures, in the range of 350 to 700 bars, while maintaining lower weight. They are also corrosion resistant. Composite tanks have been commercially available and proved for a long time. However, they are costly, considering the amount of hydrogen that can be stored in them.

3.1.3.2 LIQUID Hydrogen

Cryogenic Liquid Hydrogen (LH₂)

Liquid hydrogen has a much bigger energy density that pressurized gas. High storage density at lower pressures that gas. It needs to be contained in an insulated cryogenic tank, and to put it in there, a great amount of energy is needed. The liquefaction process, the insulated containers and the boil-off re-capture systems are the main challenges for R&D on LH2.

3.1.3.3 SOLID Hydrogen

It's a very promising technology. Storage in solid materials is safe and efficient, is needs a lower volume, lower pressure and offers a more pure output than gaseous or liquid storage. However, it requires extreme temperatures to operate, either cryogenic or very high, depending on the specific technology. More R&D needs to be done before it becomes an interesting option for a situation like the one being studied in this project, mainly due to heat management issues. Some of the options for solid hydrogen storage are:

- Rechargeable Hydrides
- Carbon and other high surface area materials
- H2O-reactive Chemical Hydrides
- Thermal Chemical Hydrides

Comparison Table 11:

Table 11: Comparison of hydrogen Storage systems

Technology	GASEOUS	LIQUID	SOLID	
Benefits	Ambient temperature Safe Simple technology Available Cheapest	Lower pressure	Lower pressure Safest	
Challenges	Higher pressure Possibility of burning if there leakage accumulates	Needs cryogenic temperatures (big energy demand) Tank must be isolated Expensive	Needs heat to release the hydrogen (big energy demand) Expensive Undeveloped technology	

3.1.4 Choice: Pressurised Gas Tank

3.1.4.1 Different PRESSURISED GAS TANKS

Customized hydrogen gaseous steel tank. Assumed fuel cell efficiency is 45%.

Then for different FC productions (Table 12), (Table 13):

Fuel cell power	Backup time	Total energy	Energy from H ₂ ^[1] @STP ^[2]	H ₂ volume @STP ^[2]	H ₂ tank ^[3] Pressure	H ₂ tank ^[3] Size
(kW)	(h)	(kWh)	(kWh)	(liter)	(bar)	(liter)
1	168	168	373	106667	30	3881
2	168	336	747	213333	30	7762
3	168	504	1120	320000	30	11643
4	168	672	1493	426667	30	15525
5	168	840	1867	533333	30	19406
6	168	1008	2240	640000	30	23287
7	168	1176	2613	746667	30	27168
8	168	1344	2987	853333	30	31049
9	168	1512	3360	960000	30	34930
10	168	1680	3733	1066667	30	38812
11	168	1848	4107	1173333	30	42693
12	168	2016	4480	1280000	30	46574

Table 12: PRESSURISED GAS STEEL TANK size depending on the FC power:

[1]. Energy Density of H2 (STP) = 3.2 - 3.5 Watt-hours/liter

(Stuart Island Energy Initiative, n.d.)

[2]. STP = standard temperature/pressure = 0°C (32 F) and 1 bar (≈1 atmosphere)

(Stuart Island Energy Initiative, n.d.)

[3]. H₂ tank pressure and size are calculated at 25°C. Actually temperature doesn't matter. Because in the ideal gas law, the temperature unit is Kelvin, 0°C = 273 K, 25°G=298 K. The ratio of these two Kelvin temperature is always close to 1, so this doesn't affect the equation.

Application	H ₂ tank
Smaller needs concept (<=3.5 kW)	ReliOn T-2000 [®] 4kW Outdoor Configuration
Bigger needs conpcet (3.5 to 5 kW)	Dantherm DBX5000
Mickelsörarna (4.4 kW)	Dantherm DBX5000
Valsörarna (5kW)	20000 liters H₂ @ 30bar,25 ºC

3.1.5 Hydrogen Utilization

Fuel cells are the best way to convert the chemical energy stored in hydrogen into electricity efficiently. There is a wide variety of fuel cell technologies already commercially available which have been proved to work satisfactorily both in stationary and mobile applications. The basics of the fuel cell imply few or no moving parts, making maintenance an unimportant issue. They are scalable, meaning that one can have from a small number of cells to a large stack of them, depending on the power delivery needed. Efficiencies for fuel cells go from 35 to 60 when used only for electricity production, but can grow up to 85 or 90% if used in CHP (combined heat and power) systems. Fuel cells have very low emissions, and since there is no combustion process, there is no emission of NOx or SOx. Also they produce very low noise and vibrations, if any, due to their lack of moving parts.

Following there is a review of the most used fuel technologies exposing the main characteristics of each:

3.1.5.1 POLYMER ELECTROLYTE MEMBRANE (PEM)

PEMs, also called Proton Exchange Membrane FC, have high power density, operate at low temperatures (around 80°C), so they can start-up quickly (short warm-up time), and can quickly vary the output to fit the needs. They have low weigh and volume. PEMs use a solid polymer as an electrolyte and carbon electrodes containing platinum catalyst, which is very sensitive to CO. They are suitable for light-duty applications (cars, buildings...). It makes them an ideal replacement for rechargeable batteries.

3.1.5.2 ALKALINE (AFC)

Alkaline FC were the first to be developed. Wide range of operating temperatures for different models (from 20 to 250°C). They use a potassium hydroxide in water as electrolyte, making possible the use of non-precious metals as catalysts. They are very sensitive to carbon contamination.



3.1.5.3 PHOSPHORIC ACID (PAFC)

Widely used nowadays. They use liquid phosphoric acid as the electrolyte and carbon electrodes containing platinum as catalysts. They operate at about 175°C. Fuel flexibility (can work with good tolerance of impurities in hydrogen, up to 1.5% of CO).



3.1.5.4 MOLTEN CARBONATE (MCFC)

MCFCs operate at high temperatures around 650°C. They require an input of CO2. The electrolyte used is a molten carbonate salt mixture suspended in an inert matrix and don't need precious metals as catalysts, due to the high temperatures. Used in big power production systems, up to a few MW.

3.1.5.5 SOLID OXID (SOFC)

SOFCs operate at very high temperatures, up to 1000°C. They use a hard non-porous ceramic compound as electrolyte and they tolerate well sulfurs presence and also CO, which can even be used as fuel. SOFC can be built in shapes other that the plate-like typical configuration. They are still quite a young technology. They are scalable and suitable for stationary applications.

(U.S. Department of Energy, Energy Efficiency & Renewable (EERE), 2011)



Below a table with the main data, applications, advantages and disadvantages of each fuel cell type or technology is shown Table 14:

Table 14: COMPARISON OF FUEL CELL TECHNOLOGIES

	Preserved Energy E Renewat	fficiency & de Energy	FUEL CELL TECHNOLOGIES PROGRAM				
Comparison of Fuel Cell Technologies							
Fuel Cell Type	Common Electrolyte	Operating Temperature	Typical Stack Size	Efficiency	Applications	Advantages	Disadvantages
Polymer Electrolyte Membrane (PEM)	Perfluoro sulfonic acid	50-100°C 122-212° typically 80°C	< 1kW-100kW	60% transpor- tation 35% stationary	 Backup power Portable power Distributed generation Transporation Specialty vehicles 	 Solid electrolyte re- duces corrosion & electrolyte management problems Low temperature Quick start-up 	Expensive catalysts Sensitive to fuel impurities Low temperature waste heat
Alkaline (AFC)	Aqueous solution of potassium hydroxide soaked in a matrix	90-100°C 194-212°F	10-100 kW	60%	• Military • Space	Cathode reaction faster in alkaline electrolyte, leads to high performance Low cost components	Sensitive to CO ₂ in fuel and air Electrolyte management
Phosphoric Acid (PAFC)	Phosphoric acid soaked in a matrix	150-200°C 302-392°F	400 kW 100 kW module	40%	Distributed generation	Higher temperature enables CHP Increased tolerance to fuel impurities	 Pt catalyst Long start up time Low current and power
Molten Carbonate (MCFC)	Solution of lithium, sodium, and/ or potassium carbonates, soaked in a matrix	600-700°C 1112-1292°F	300 kW-3 MW 300 kW module	45-50%	Electric utility Distributed generation	High efficiency Fuel flexibility Can use a variety of catalysts Suitable for CHP	 High temperature corrosion and breakdown of cell components Long start up time Low power density
Solid Oxide (SOFC)	Yttria stabi- lized zirconia	700-1000°C 1202-1832°F	1 kW-2 MW	60%	Auxiliary power Electric utility Distributed generation	High efficiency Fuel flexibility Can use a variety of catalysts Solid electrolyte Suitable for CHP & CHP Hybrid/GT cycle	High temperature cor- rosion and breakdown of cell components High temperature opera- tion requires long start up time and limits

(U.S. Department of Energy, Energy Efficiency & Renewable Energy (EERE), 2011)

3.1.6 Choice: Fuel Cell

• Different FUEL CELLS (Table 15, Table 16):

Table 15: Comparison of PEM Fuel Cells

Product	H ₂ flow rate (l/h)	H₂ purity (%)	H₂ pressure (bar)	Power output (W)	Comments / Reasons for discarding	
GreenHub 500	390	99.999	4-8	0.4 kW		
GreenHub 1000	840	99.999	4-8	0.8 kW	Fuel-cells of greenhub	
GreenHub 2000	1680	99.999	4-8	1.6 kW	gensets are not designed	
GreenHub 3000	2520	99.999	5-8	2.55 kW	for a continuous 24/7	
GreenHub 4000	3600	99.999	7-10	3.4 kW	running profile	
GreenHub 5000	5040	99.999	7-10	4.25 kW		
Fronius 50F	3300	99.999	5-15	4 kW	Too high purity, ambient temperature is higher than +3ºC	
Dantherm DBX5000	4750	99.95	6	5 kW	Meets the electricity needs of both islands, can operate below -20°C	
ReliOn T2000	1800	99.95	0.24-0.41	2 kW	Scalable, flexible config. from 600 Watts to a full 2000 Watt capacity	
ReliOn T2000 4kW Outdoor		99.95		4 kW		
ReliOn T2000 6kW Outodoor		99.95		6 kW	Modular configurations, can work at ambient temp. from -40ºC to 46°Ç high reliability, ease of maintenance, simplicity of design	
ReliOn T2000 Outodoor		99.95		8 kW		
ReliOn E2500 10kW 32U23 Cabinet		99.95		10 kW		
ReliOn T2000 12 kW Outdoor		99.95		12 kW		

Table 16: PEM FUEL CELL choice for each application:

Application	Туре
Smaller needs concept (<=3.5 kW)	<15000 liters H ₂ @ 30bar, 25 ^a C
Bigger needs conpcet (3.5 to 5 kW)	15000-20000 liters H₂ @ 30bar, 25ªC
Mickelsörarna (4.4 kW)	20000 liters H₂ @ 30bar, 25ªC
Valsörarna (5kW)	20000 liters H ₂ @ 30bar, 25ªC
3.2.1 Heating System Trade-Off



Figure 8: Heating System Trade-Off

3.2.2 Ventilation System Trade-Off



Figure 9: Ventilation System Trade-Off

3.2.3 Explanation of different criteria.

Criteria	Explanation
Efficiency	A percentage as a result of what is actually performed by a system, with what can be achieved with the same consumption of resources. High percentage, gives a better score.
Investment costs	The initial fee one has to pay for installing the complete system. Low price, gives a better score.
Installation costs	The cost to place and install system . Transportation costs are taken into account. The cheaper it is to operate the solution, the better is the score.
Reliability	The ability of a system to perform its intentional function without failing. This is often expressed as mean time between failures. If the time between failures is long, the score will be high.
Maintenance	Actions necessary for repairing or restoring a piece of equipment, machine, or system to the specified condition. This to maximize its useful lifetime. The lower the maintenance needed, the higher the score.
Lifetime	The time in which the system is running without replacing it. The longer the lifetime, the higher the score
Visibility	The capability of providing a unobstructed view, clear from all equipment, machines, or systems. If the system is affecting the view of the landscape, the score will be low
Seasonal influence	Influence that the seasons have on the system and its operation. A low seasonal influence, gives a high score.
Environmental impact	The way an installation and its operation affects the ecosystem. Low level of damage, gives high score.
Humidity control	Capacity of the system to control the humidity inside the building. High control capacity, gives high score.



ENERGY STAR HIGH EFFICIENCY HAUTE EFFICACITE until



THE ZUBA-CENTRAL HEAT PUMP

AV.

Cooling

Heating

In summer, heat pump works like an air conditioner which cools your home by moving heat from indoor through the air handler to outdoor.

uuu In winter, heat pump works in reverse. It absorbs heat from the outdoor air and moves it indoor to warm up your home.

OUTSTANDING PERFORMANCE

Zuba-Central's unique Hi technology has you covered even during the coldest winter days.

						Traditional Heat Pump
Zuba Cent	ral					
		1	1	Ambi	ient temperati	ure 'C ['F] (W.B.)
-30 [-22]	-25 [-13]	-20 [-4]	-15 [5]	-10 [14]	-5 [23]	0 [32]

Zuba-Central is a Heat Pump which provides heating and cooling to your home through ductwork. It is ranked among the most energy-efficient and cost-effective ways of transferring heat from one place to another.

Compared to other means of heating, heat pumps are very efficient, but only as long as outside temperatures stay above 0°C. From this point and below, a supplemental heating system has to be used.

Now with Zuba-Central, not only will you get the benefits of a heat pump above 0°C, but all the way below!

HYPER-HEAT INVERTER (H²i)

The secret behind Zuba-Central's high-heating performance, even under extremely low outdoor temperatures, is our exclusive Hyper-Heat Inverter (H^zi) technology. It maximizes the benefits and efficiencies you can get from a heat pump.

In addition, the unique defrost mechanism - which prevents automatic defrosting when not required - gives the system a quick start-up time and provides continuous heating.

EFFICIENTLY GREEN

Thinking Green Has Never Been So Efficient.

Now you can keep more money in your pocket while reducing your carbon footprint. The Zuba-Central system uses ozone-friendly R-41 0A refrigerant which produces no CFCs or HCFCs, and has zero Ozone Depletion Potential (ODP). This is not only beneficial to the environment but also translates into better overall performance and energy efficiency than traditional R-22 based systems.

Through the use of our VSCI Technology (Variable Compressor Speed Inverter) the Zuba-Central system is able to dynamically adjust heating and cooling capacities to match actual requirements of your home, which means you pay only for the required energy when you need it.



Zuba-Central is an Energy Star® qualified heat pump with a SEER1 of 15.0 in cooling mode and an HSPF2 of 9.4 in heating mode. Together with a high-efficiency ECM motor, you can be sure that you're always getting the most from your utility bill and giving the most back to the environment.

1. SEER & easonal Energy Efficiency Ratio) 2. HEPF (Heating Seasonal Performance Factor)



THE ADVANTAGES OF EVOLUTION

TECHNOLOGY YOU CAN TAKE TO THE BANK



Editorial Annual Husting Costs (Savings) for a tigotal houre with calculated hour into all 60,000 Plu/h (append 2,000 sqt)** ("Note: Mitsubint Electric Dates Canada inc, provides these figures without including obligation or labits, Figures may vary depending on application. For an accurate account of potential calego Mitsubint Electric Canada recommends a through energy and to be completed by a guilted date or technicial.

TINY FOOTPRINT, MASSIVE IMPROVEMENT

SLIMMER THAN A BACKYARD TILE.

The Zuba-Central outdoor unit measures only 13 inches (33 cm) thick – which sits perfectly alongside your exterior wall and takes up a lot less real-estate than a traditional A/C system. It is so compact that you can have it installed anywhere around your premises without taking up your valuable patio space.

The indoor Air Handling Unit is smaller than a gas furnace, and fits right onto your existing ductwork. Everything is efficiently housed in a single unit.

QUIETLY OUTPERFORMING

YES. IT'S RUNNING!



You may not even realize your Zuba-Central system is hard at work keeping temperatures steady and bringing you home comfort. Our advanced technology ensures super-quiet units that work vibration-free.

Whispe

As low as 52dB(A)

Zuba-Central

40dB(A) Dulet photo studio	SOdB(A) Mid rainfal	55dB(A) Business machines	65dB(A) Fan	70dB(A) Refrigerator	75dB(A) Haindryer	80eBi Stansia A/C Lin

HOW MUCH AM I REALLY SAVING AND WHAT DO ALL THE NUMBERS MEAN?

Coefficient of Performance (COP) is a standard measurement of how much energy you get out of every unit of fuel input. The higher the number, the more savings you can get from your utility bill.

COP Zuba: 1.4 - 3.19 Gas: 0.95 Electric: 1.0

Even the most efficient gas furnaces only provide fuel efficiencies of up to 95%, or COP of 0.95. And for electric resistance heaters, their COP equals 1.

Zuba-Central's OOP ranges from 1.4 to 3.19, depending on the outside temperature. It actually gets more efficient as temperatures increase!

ľ

OUTDOOR UNIT

PATIO TILE



MITSUBISHI ELECTRIC Changes for the Better

ZUBA-CENTRAL IS SIMPLY THE NEW AND BETTER WAY TO PROVIDE YEAR-ROUND HEATING & COOLING COMFORT. MADE FOR CANADA, THIS EASY-TO-INSTALL. MONEY AND SPACE-SAVING SYSTEM WILL FOREVER CHANGE THE WAY YOU EXPERIENCE HEATING & AIR CONDITIONING.

Madel		Zuba-Central
Caaling	Max, Capacity	36,000 Btu/h
	Max. Input	3,165 W
	EER	11.50
	SEER	15.00
System Operating Temperature Range - Cooling	Indoor	D.B. 88 - 90°F (19 - 32°C) W.B. 59 - 73°F (-15 - 23°C)
	Outdoor	D.B. D-115*F (-18-46*C)*
Heating	Max. Capacity	40,000 Btu/h
	Max. Input	3,670 W
	HSPF	9.4
System Operating	Indoor	D.B. 63 - 83°F (17 - 28°C)
Temperature Range - Heating	Outdoor	D.B22 - 70°F (-30 - 21.1°C) W.B22 - 59°F (-30 - 15°C)

"with wind haffle

ZUBA-CENTRAL +

The optional Zuba-Central+ even has you covered in those rare instances when extreme temperature hits the air. It can be equipped with your choice of an auxiliary Electric Resistance Heater or Hydronic Hot Water Coll that operates simultaneously with Zuba-Central only when additional heat is needed. So even during the coldest days, your Zuba-Central+ package is still pumping heat indoors with the superb efficiency that only a heat pump can offer.

Zuba-Central+ is available with Electric Resistance Heater option from 2.5kW to 17.5kW, or with 2 or 3-row Hydronic Hot Water Coll option with or without pump. It is also available with SCR duct heater option for enhanced efficiency. Please ask your local dealer which option best meets your requirements.

5-YEAR PARTS WARRANTY 6-YEAR COMPRESSOR WARRANTY

Vancouver and Taronto energy costs are estimated based on \$0 x0/m² for natural gas and \$0.08W/m for electricity. Montheal energy costs are estimated based on \$0 x0/m² for matural gas and \$0.07W/Wh for electricity. *Cost oscialation astimated based on a gas furnacewith COP of 0.55.1 Direct calculation estimated based on a Zube-Dentral system with a 10xW apprementary tester which only operates whenhead loss cannot benere by Zube-Dentral stone.









www.Zuba-Central.ca

TAS-2016/11-E Misubit/Elastic reserves the right to modify the design of its products, their characteristics and the information contained in this iterature. Specifications are subject to charge without notion.

(ZUBA-CENTRAL, 2008)



3.3 Appendix 13: Sensors Diagram

Figure??: SENSORS DIAGRAM

4 Results

4.1 Appendix 14: Wind Turbine Datasheet





安徽蜂鸟电机有限公司 ANHUI HUMMER DYNAMO CO.LTD

3. Specifications

Rated power (W)	10000
Maximum output power (W)	15000
Battery bank voltage (Vdc)	240
System output voltage (Vac)	110/220/380
Start-up wind speed (m/s)	3
Rated wind speed (m/s)	10
Working wind speed (m/s)	3-25
Survival wind speed (m/s)	50
Generator efficiency	>0.85
Wind energy utilizing ratio (Cp)	0.4
Generator type	Permanent Magnet Alternator
Generator weight (kg)	287
Blade material/quantity	GRP/3
Blade diameter (m)	Φ8.0
Speed regulation method	Yawing+Electromagnetism braking (Optional hydraulic braking)
Shutting down method	Manual+Automatic

4. Structural Pictures and Description

Generator body: mainly including generator, nose cone, and protection cover

Hummer generator, the most advanced in the world, wins 4 proprietary intellectual property rights. It is made of high-efficiency magnetic materials, special copper alloy, high-strength stainless steel and aeronautic aluminum alloys. It is extremely light and small but with high power generating efficiency.



Nose cone

Made of reinforced aluminum alloy, it locates in front of blades to reduce the wind resistance. The generator is enclosed in the nose cone, which is favorable for heat dispersion.

Protection cover

Made of reinforced aluminum alloy, it locates between blades and nose cone to further reduce the wind resistance and protect the generator.



SKF Bearings

Two SKF bearings, famous in the world with good quality and a long history, make sure the system in reliable, safe and steady operation status.



Flange

Made of fine steel parts, it is used to fix the blades.



Blades

Made of glass reinforced plastic, they receive wind energy and convert it into mechanical energy. Every 3 blades compose one set and pass strict balance test before delivery, so please don't disorderly use.



Yaw shaft

Made of fine steel parts, it is used to connect generator and blades with tower together. With 24V power supply and gear box included, it controls the operation of wind turbine.



Off grid inverter

Adopting SPWM technology, it will inverter with high converting efficiency, output stable frequency and stable voltage, filter out noise. It is used in the off grid system and power the electric loads.



安徽蜂鸟电机有限公司 ANHUI HUMMER DYNAMO CO.LTD



Grid tied inverter

Adopting MPPT and IGBT technologies, it inverters with high power generating capacity and wide AC voltage range. It connect with state grid and the energy storing device isn't needed.



PLC controller

As adopting Siemens CPU the technology of touch screen, it will alarm automatically and regulate the operation situation of wind generator. Users can also set the parameters according to actual needs.



Rectifier/ dumping controller

It rectifies AC current generated by wind generator into DC current and charge the battery bank. It also controls the dumping load.



(Anhui Hummer Dynamo Co., Ltd., 2011)

TECHNICAL DATA SHEET AB190M、AB195M、AB200M

Technical Data	
Type	AB190M, AB195M, AB200M
Type of Solar Cell	Mono-crystalline, 125mm×125mm
Number of Cells	72 pcs
Size of module	1580×808×40mm
Module, Weight	15 kg
Connector / Cross-Section	GZX
Cables, Length (+/-)	900mm 4mm ² Cable with polarized waterproof DC
Front Cover Glass	3.2mm Hight Light Safety Glass
Packaging materials	EVA,Polyester
Frame	Silver Anodized Aluminium

Electrical Data				
Maximum Power	P MPP STC	190 W	195 W	200 W
Power Tolerance	Δ _{stc}	+/-3%	+/-3%	+/-3%
Maximum Power Voltage	U MIP STC	36.7 V	36.8 V	37.0 V
Maximum Power Current	I MPP STC	5.18 A	5.30 A	5.41 A
Open Circuit Voltage	Uacistic	44.8 V	45.0 V	45.2 V
Short Circuit Current	I _{SC STC}	5.51 A	5.59 A	5.68 A
Cell Efficiency	η _{stc}	17.1 %	17.5 %	17.9 %
Maximum System Voltage	U _{DC}	1000V	1000V	1000V

STC: Irradiance 1000 W/m²; Spectrum AM 1,5; Cell Temperature 25°C, Wind 0 m/s



Temperature Coefficients				
Power Coefficient	a _k (P _{see})	- 0.47 %/K		
Voltage Coefficient	$\beta_k (U_{oc})$	- 0.35 %/K		
Current Coefficient	$\phi_k(I_{sc})$	0.065 %/K		

Power Warranty

10 years performance warranty to 90 %

25 years performance warranty to 80 %

5 years warranty against production and material defects

Certifications

TUV, CE, ISO9001:2008

(Xuzhou Aibo Energy Technology Co., Ltd, 2012)



Overview

Quiet48-5 is Telgenco's ultra quiet 5kW 48V DC diesel powered battery charging system. Quiet48-5 provides over 100 amps of clean DC output to plug directly into an existing 48V battery bank or to replace it altogether with Quiet48-5 internal battery bank.

The Quiet48-5 is designed primarily to provide DC power for communications sites in urban environments or remote rural areas. The standard Quiet48-5 system includes diesel engine, fuel tank, battery bank and Remote Power Controller housed within a vandal resistant acoustic enclosure. The acoustic design is integral to all Telgenco gensets, our philosophy is to make the Quiet48-5 at full operating speed quieter than a modern diesel engined car at idle. This allows Quiet48-5 to be deployed in locations where conventional gensets would cause a noise nuisance. The Quiet48-5 also has a number of integrated component options including a solar PV charging controller, a mains powered rectifier and an AC supply inverter (for dual AC/DC output). These options are all integrated with the remote control system and central software providing operators of the system with unrivalled visibility of the site power status. The options can save operators money and reduce the number of descrete boxes on a site. All the optional components are housed within the Quiet48-5 vandal resistant enclosure improving overall site security.

Key Benefits

The Quiet48-5 is a state of the art system with a number of key benefits over more conventional generators. Key benefits include:

- · Automated remote control
- Full engine monitoring and control
- · Predictive maintenance logging and alerting System alarms optionally delivered via SMS and email
- Internal UMTS/GPRS wireless modem with GPS
- · Extremely quiet operation
- · Clean 48V DC output
- · Integral 48V battery bank
- · leak free bunded internal fuel tank
- · Rugged vandal resistant construction
- 100% Biofuel engine option
- · Integrated solar PV charging option

Telgenco Remote Generator

Monitoring and Control

- Integrated mains rectifier option



Remote Power Controller

The Telgenco Remote Power Controller is mounted within the Quiet48-5 enclosure. It monitors and manages a wide range of critical engine and fuel system parameters as well as generator site security.

The Remote Power Controller interfaces back to the Telgenco Remote Management Server via fixed IP, satellite or the built-in 9 Band UMTS/GPRS modem. For Mobile or rental environments the Remote Power Controller also provides accurate GPS based position reporting for asset tracking.

The Remote Power Controller undertakes multiple management functions in the Quiet48-5 including:

- Auto start management Fuel system monitoring & reporting
- Lubrication system monitoring & reporting
- Cooling system monitoring & reporting Filter conditions monitoring & reporting
- Engine and environment temperature monitoring & reporting
- Recording engine hours
- Security monitoring & reporting Unauthorised system movement detection
- DC charging management
- Battery condition management Genset voltage control
- Geographic location reporting
- Video monitoring of genset site Remote communications and monitoring of solar PV and other renewable controllers

The flexible design of the Remote Power Controller allows additional bespoke monitoring functionality to be easily added.





Battery Protection

From the outset the Quiet48-5 has been developed to provide a safe and controlled system for charging DC battery banks. The system monitors the battery voltage, the battery temperature and the load current and uses internal algorithms to provide the correct amount of voltage into the battery bank for the given conditions. The algorithms control the engine speed 50 times per second to vary the voltage to the appropriate level. Varying the engine speed according to load also has the advantage of saving fuel. In addition to the software control there are built-in hardware protection circuits to ensure that the battery bank is not overcharged under any circumstances.



Renewable Energy Integration

The Quiet48-5 has been designed from the outset to be easily integrated into a renewable energy solution. The Quiet48-5 can be supplied with an optional 48V solar PV charging controller with either a 4kW or 8kW solar capacity. This controller is integrated with the Remote Power Controller to provide full remote visibility of the entire system including solar output and battery status. When the power demand is not met by the solar output or the energy stored in the battery bank the Quiet48-5 automatically starts its diesel alternator.

The Quiet48-5 has a 100% biofuel compatible engine option, this allows the system to be used as a totally hydrocarbon free renewable energy exchange with consequent environmental benefits.

Rugged and Ultra Quiet Construction

The outer skin of the Quiet48-5 is constructed from 3mm thick zinc coated steel plate which is polyester powder coated for lasting durability. The outer skin is designed to resist vandal and theft attacks and dramatically reduce vulnerability compared with conventional thin sheet construction. The Quiet48-5 has a 50mm thick thermal and acoustic insulation layer sandwiched between the outer skin and an internal galvanised steel skin. This significantly reduces the engine noise radiating out of the enclosure. The exhaust is passed through two sequential silencers and the intake and exhaust air travel in and out of the enclosure via acoustic silencers. This attention to sound reduction ensures that the Quiet48-5 has a SPL lower than 50 dBA at 10m.

Combined DC and AC output

While the standard output of the Quiet48-5 products is DC in some circumstances customers have some AC devices on site that they want protected from power failure. An example of this might be a communications site in a hot location where functional air conditioning is critical to the stability of the communications electronics. To accommodate this we are able to include an optional inverter to provide a proportion of the power in either 100, 110, or 240V AC. Under this scenario in the event of the incoming power failing the DC communications system and the AC cooling system will continue to function normally.



Environmental Protection and Emissions Compliance

Telgenco is committed to protecting the environment. Our Quiet48-5 are manufactured from environmentally inert materials and designed to be almost completely recycled at their end of life. The internal fuel tank is fully enclosed within a leak free bund with active leak detection and alarms. The fuel filler has an integral overfill protection system ensuring spill free refuelling. The engines we use are compliant with European and US emissions standards including Tier 4 Interim.

Warranty, Support and Finance

All Quiet48-5 systems are sold with a comprehensive 3 year warranty on parts and labour and a 7 year corrosion warranty. At the end of the warranty period there is an option to purchase an extended warranty. Telgenco provide comprehensive support and training during the installation and commissioning phase of new deployments. After installation we provide 3rd tier support to your system managers on an as required basis. For larger deployments (of 50 or more systems) we can provide a financing scheme to qualifying companies, this can spread the capital costs of systems over several years improving the project payback period.

About Telgenco

Telgenco (part of Controllis Limited) is based in the UK with headquarters in Cambridge, the heart of the Silicon Fen high-tech cluster. Controllis was founded in 2008 with a vision to provide remotely managed systems for a range of different markets. Our engineering team is made up of highly experienced engineers, software developers and technicians from the Telecommunications, Power Generation, Defence and Formula 1 Motorsport sectors. The company is privately owned and funded by the management team, a number of private investors and a UK based defence and aerospace company.

Quiet48-5 Specifications

Power Output	100 A DC at 48V to 65V
Voltage Ripple	<100 millivolts peak
Engine	Perkins 3 Cylinder 1100cc or Lister Petter 2 900cc (customer choice)
Fuel	Diesel, Indirect Injection, Up to B100 with Lister Engine Option
Built in Remote	Auto Engline Start
Power Controller	Electronic Throttle Control
	48V Intelligent Charging System
	12V Intelligent Charging System
	Battery Temperature Monitoring
	Fuel Level
	Oil Level
	Oil Filter Pressure Drop
	Fuel Filter Pressure Drop
	Air Filter Pressure Drop
	Coolant Temperature
	Oil Temperature
	Environmental Temperature
	Exhaust Temperature
	Oil Quality Sensor (Optional)
Communications	Ethernet with built-in UMTS/GSM (see Remote System Controller datasheet for full details)
Internal Fuel Tank	200 litres
	Optional external fuel tank connection
Frame Construction	All Welded Steel
Corrosion Protection	All external components galvanised or hot zinc sprayed
Paint	Oven Baked Polyester Powder Coated
Colour	Standard RAL7035 (Other colours optional)
Noise Level	<50 dB(A) at 10m free field
Emissions	EURO stage IV and EPA Tier4 Compliant
Environ mental Operating Temperature	-40C to +55C
Dimensions WxHxD	1510 x 1888 x 1100
Weight	650Kg





Contact Us

Head Office Trinity House Cambridge Business Park Cambridge CB4 0WZ United Kingdom

 Ph:
 +44 (0) 1223 393 543

 Fax:
 +44 (0) 1223 771 604

 Email:
 sales@telgenco.com

 Web:
 www.telgenco.com

(TELGENCO, 2012)

4.4 Appendix 17: Electrolyzer Datasheet





TECHNICAL DATA		AES 100	AES 200	AES 3005
H2 production rate	N/h	100	200	300
Standard working pressure	bar	15	15	15
Maximum allowable pressure	bor	30	30	30
Purity @30bar (1)	%	99.94	99.94	99.94
Purity with additional dehumifier	%	99.999	99.999	99.999
Water Consumption	l/h	0.08	0.16	0.25
Water Conductivity @ 25°C (2)	µ\$/cm	5-10	5-10	5-10
Power consumption	w	530	1060	1590
Dimension - (Ax8xC)	mm	180x190x145	180x190x225	180x190x300
Weight (without water)	Kg	11.5	16.0	20.5

Without any purification
 Demineralized / distilled water only





Acta S.p.A. Via di Lavoria, 56/G - 56040 Crespina (PI) - ITALY P.O. Box 143 - 56021 Cascina (PI) - ITALY Tel. +39 050 64 42 81 - Fax +39 050 64 22 51- info@actaspa.it - http://www.actagroup.it

4.5 Appendix 18: Fuel Cell Dantherm DBX5000 Datasheet







CONTROLLER INTERFACE:



Front panel - Valve Block, Alarm, CAN, TCP/IP & LED's - AC-input, DC-out & current sharing



TECHNICAL DATA:				
		DBX5000		
Important Note	DBX requires fresh air supply and ducting of exhaust air to outside ambient. DBX can only work when equipped with Dantherm Power Valve Block and a fuel regulator supplied by or approved by Dantherm Power			
System capacity				
Power output	We	Continuous	5000	
Voltage output	VDC	Fixed within	-47 to -57	
Voltage input	VAC	For standby operation	90 – 264 / 50-60 Hz	
Fuel				
Hydrogen purity (H ₂)	%	Commercial grade 3.5	Min 99,95	
Inlet Pressure	Barg	Nominal to Valve Block	5	
Consumption	Nm3/kWh	Average at max. load	0,95	
Physical				
Ambient Temperature	°C	Operational (optional)	-20 (-40) to +40 (-55)	
Integration cabinet Temperature	°C	Operational	0 to +60	
Storage Temperature	°C	Weather protected	-45 - +70	
Cabinet dimensions	mm	H x W x D	611 x 500 (450) x 555	
Weight	Kg	Stand alone module	75 Kg	
Ingress Protection	IP-class	External to internal	55	
Air flow	m3/h	Exhaust to outside	200-1600	
Backup start up time	sec.	Depends on batteries	Installation dependent	
Communication				
Interface/system monitoring	-	Standard configuration	RJ45 TCP/IP – CAN Bus Display panel	
Alarms				
Voltage free outputs	-	Goes open on fault	DB15 with 4 channels	
Visual indication	-	Display	1	
Interface				
DC	-	On front panel	175 Amp Anderson type	
AC (only DIB version)	-	On front panel	IEC 320 C14	
Hydrogen	Fitting	-	8 mm Tube	

Dantherm Power A/S · Majsmarken 1 · DK-9500 Hobro · Tel.; +45 88 43 55 00 E-mail: sales.power@dantherm.com · www.dantherm-power.com

Dantherm Power Inc. · 4260 Orchard Park Blvd. · Spartanburg, SC 29303 · USA · Tel.: +1 (864) 595 9800 · Fax: +1 (864) 595 9810 E-mail: sales.power@dantherm.com · www.dantherm-power.com

4.6 Appendix 19: Fuel Cell ReliOn T2000 Datasheet



T-2000 Hydrogen Fuel Cell

Functional Diagram



Product Specifications

riouuci opecifications		T-2000®	T-2000 [®] in Enclosure				
Physical	Dimensions (w x d x h)	21"x 21.5" x 26"	Modular configurations				
		53.3 cm x 54.6 cm x 66 cm	availa ble				
	Weight	134 to 244 lb s / 61 to 110 kg					
	Mounting	23" rack mount					
Performance	Rated net power	0 to 2,000 Watts	0 to 12,000 Watts				
	Rated current	0 to 80A @ 24VDC / 0 to 40A @ 48VDC					
	DC voltage	24 or 48 VDC nominal					
Fuel	Composition	Standard industrial grade hydrogen (99.95%)					
	Supply pressure to unit	3.5 to 6 psig / 24 to 41 KPag					
		0.24 barto 0.41 bar					
	Consumption	30 slpm @ 2000 Watts					
	Hydrogen Storage Capacity	n/a	Modular solutions scalable				
			from 48 to 96 kWh				
Operation	Ambient temperature	35°F to 115°F / 2°C to 46°C	-40°F to 115°F / -40°C to 46°C				
	Relative humidity	0-95% non-condensing					
	Altitude	-197 ft to 13,800 ft / -60m to 4,206m					
	Location	Indoors	Outdoors				
Safety	Compliance	UL/CSA/CE	NEBS Level 3 / Seismic Zone 4				
Emissions	Water	Max. 30mL / kWh					
	Noise	53 d BA @ 3 28 ft / 1 meter					
Monitoring / Control	Remote	System configuration & status / Historical & operational data					
	Communications RJ 45 / DB9 / Dry Contact						



(ReliOn, Inc., 2008)

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NEBS Level 3

Corporate Offices

15913 E. Euclid Ave. Spokane, WA 99216 Tel: 1-509-228-6500 Toll Free (U.S.): 1-877-474-1993 Fax: 1-509-228-6510 www.relion-inc.com





Products	E-200	E-1100	E-1100v	E-2500	T-1000	T-2000	Telecom	Government	Off-Grid	Transportation	Utility	Certifications

PRODUCTS & SOLUTIONS

T-2000 | T-2000: 2kW Outdoor Configuration | T-2000: 4kW Outdoor Configuration T-2000: 6kW Outdoor Configuration | T-2000: 8kW Outdoor Configuration T-2000: 12kW Outdoor Configuration

T-2000® 4kW Outdoor Configuration

sectors. For customers looking for < 1000 Watts to The T-2000® outdoor configurations are designed 4,000 Watts of backup power, the T-2000® 4kW outdoor configuration provides the flexibility and for larger communications backup power loads telecommunications, utility and government higher outputs needed for a variety of site within the wireless and wireline requirements.

5

Tax Incentives

Features:

- 48kWh Hydrogen Storage Cabinet
 - Site loads ranging from 0 4kW
- Output: 0 to 4,000 Watts 24 or 48 VDC nominal
- output
- 12 + hours of fuel storage
- Expandable to 12 cylinder capacity for 24 + hour runtime
 - Remote Monitoring Capability
- Dimensions: 72"h x 54"w x 41"d (183cm x 137cm x 104cm)
 - Fuel: Industrial Grade Hydrogen





4,000 Watt - 48 kWh Configuration

4.8 Appendix 22: Gebwell T GSHP technical datasheet

HVAC circuit diagram example



Carefree and reliable

The T ground source heat pump is a carefree and reliable heating solution, which guarantees an even and pleasant room temperature and sufficient domestic hot water. By connecting two heating control groups to the ground source heat pump, you can heat damp spaces year-round regardless of the individual heating requirements of other spaces, for example.

Correct dimensioning maximises the benefits of the ground source heat pump and minimises the expenses. Gebwell dimensioning takes care of heating, comprehensively and efficiently.

Compact and polished

The Gebwell T ground source heat pump has a light, compact structure and a clean, polished look. The design and realisation seek to ease the installability and operability of the pump, which are one of a kind in the T ground source heat pump.

The T ground source heat pump is an excellent solution for heating detached houses, terraced houses and small apartment blocks and for preparing domestic hot water. It is suitable for both new and renovated buildings, and can be connected to radiator heating as well as underfloor heating.

Phases of the ground source heat

delivery Gebwell Ltd. and its partners deliver ground source heat

turnkey solutions:

- · Planning and full capacity dimensioning
- Selecting and performing heat collecting circuit implementation
- · Heat well drilling service
- · Required ground work and leading-through
- Installing the heat pump
- · Installing a property heating and domestic water network
- Implementation and introduction
- · Inspecting and accepting the installation

Ease of installation

- · The heating group that is delivered as an accessory can be connected to the heating network effortlessly
- · The ground loop valve group is compact, and makes deaeration faster
- · The hauling of a ground source heat pump is very easy.

Gebwell T ground source heat pump benefits

- · Providing environmentally friendly heating energy at · Finnish-built with high-quality a stable cost
- · Carefree and easy to use heating system
- · Long lasting, reliable product that is manufactured using high-quality components and is covered by a warranty
- The unit can be expanded using ready modules
- · An adequate amount of fresh and warm domestic water with the super heating technique
- · Available accessories include a GSM modem, for example
- · Maintenance contract/extended warranty service concept
- · Optimised products for different power ranges

The Gebwell T ground source heat pump is a heat pump unit that is to be connected to a separate accumulator (for example, Gebwell G-Energy HP accumulators), which is suitable for new buildings and especially renovated buildings. The T ground source heat pump is also suitable as a producer of extra heat alongside other systems.

G-Energy HP accumulators

 Superheating accumulator collection (500-3000 I), which is meant to be connected to the T model heat pump units, is suitable for destinations with a large momentary need for domestic water.

Gebwell extension modules help ensure the quick installation of the needed pipe connections.

- The ground loop valve group contains the necessary valves, reversing valves and mud separator.
- The heating control group contains a rotary pump and a control valve with operational devices for one heating circuit.

Technical specifications

Gebwell T EAN number	T6 6415853619240	T8 6415853619257	T10 6415853619264	T12 6415853619271	T15 6415853619288	T20 6415853619295	T25 6415853619301	T30 6415853619426
Heating output kW (0°/35°C)	6	8	10	12	16	22	26	32
Compressor	Scroll	Scroll	Scroll	Scroll	Scroll	Scroll	Scroll	Scroll
Voltage	3~400 V	3~400 V	3~400 V	3~400 V	3~400 V	3~400 V	3~400 V	3~400 V
Fuses, A	3x16	3x16	3x16	3x16	3x20	3x25	3x32	3x40
Refrigerant	R407C	R407C	R407C	R407C	R407C	R407C	R407C	R407C
Recommended size for back-up resistor	6	6	6	6	9	12	15	15
resistor located in the accumulator								
Buit-in heat collecting/heating pump								
Dimensioning								
recommendations								
Heated area, m ⁺	<120	<170	<200	<240	<330	<460	<700	850
Heat collecting piping	<400	<450	2x200/2x300	2x300/2x400	2x400/3x300	3x300/3x500	3x400/4x500	3x500/4x500
(body of water/ground)								
Total depth of bored well, m	<120	<160	<180	2x110	2x130	2x190	3x160	4x150
Dimensions								
Height	1100 mm*	1100 mm*	1100 mm*	1100 mm*	1100 mm*	1100 mm*	1100 mm*	1100 mm*
Width	596 mm	596 mm	596 mm	596 mm	596 mm	596 mm	596 mm	2 x 596 mm
Depth	642 mm	642 mm	642 mm	642 mm	642 mm	642 mm	642 mm	642 mm
Weight	100 kg	100 kg	100 kg	100 kg	150 kg	150 kg	150 kg	300 kg
Colour	White, inquire about other colour options adjustation of the region of t							
Extension modules Ground loop valve group Heating control group						States	RI	
G-Energy HP superheating act EAN number	cumulator	5 00 l 6415853619431	1 000 I 6415853619448	2 000 l 6415853619455	3 000 l 6415853619462			
Height (+ adjustable feet 0-60 mm)		2050 mm	2150 mm	2200 mm	2350 mm			







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We reserve the right to carry out possible dimensional and structural changes!

v.1-0 11062010

(Gebwell Ltd., 2010)

EN-

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